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NAC: NEUTRON ACTIVATION CODE

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ABSTRACT

NAC is a computer code designed to predict the neutron-induced gamma ray radioactivity for a wide variety of composite materials. This code is a subset of the NAP code, and the code output has been altered to provide convenient analysis by experimenters. The NAC output includes the input data, a list of all reactions for each constituent element, and the end-of-irradiation disintegration rates for each reaction. The code also compiles a product isotope inventory containing the isotope name, the disintegration rate, the gamma-ray source strength, and the absorbed dose rate at 1 meter from an unshielded point source. The induced activity is calculated as a function of irradiation and decay times; the effect of cyclic irradiation can also be calculated.

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SUMMARY

NAC is a computer program designed to predict the neutron-induced gamma ray radioactivity for a wide variety of composite materials. The unshielded induced radioactivity is calculated as a function of neutron exposure and decay times. The effects of cyclic exposure to a neutron flux and target atom burn-up can also be calculated.

E-4447

NAC, a subset of NAP, provides fewer computational options than NAP and the output has been altered to provide for more convenient analysis by experimenters. The NAC output includes the input data, a list of all reactions for each constituent element, and the end of irradiation disintegration rates for each reaction. The code also compiles a product isotope inventory containing the isotope name, the disintegration rate, the gamma ray source strength, and the absorbed dose rate at one meter from an unshielded point source. A breakdown of the above data as a function of gamma energy for each product isotope is available as an option.

INTRODUCTION

NAC is a computer code written to provide a means of rapid analysis of the neutron-induced gamma ray radioactivity for a wide variety of composite materials. The code is a simplified version of the NAP program (see ref. 1). NAP was written to calculate the induced activity and unshielded gamma dose as a function of time, space, and gamma energy. NAP was designed to use the neutron spectrum output from a transport code and to provide input data for a gamma shielding code. NAP is highly versatile and well suited to this type of activation calculation. However, the detailed calculations available with NAP are not warranted in experimental situations in which knowledge of the neutron spectrum is limited and the activation information required is minimal. Such a situation would occur

when the knowledge of the post-irradiation activation hazards of an experimental capsule, to be irradiated in a test reactor, is desired.

NAC was written to provide this type of activation calculation, and the code output has been designed to provide for convenient analysis by experimenters. The output consists of two sections. The first contains the input data (material composition, neutron fluxes, irradiation time, a list of the reactions considered for each element, the end of irradiation disintegration rates (dis/sec) for each reaction, and the fraction of the activity produced by each neutron energy group. The second section is a product isotope inventory containing the product name, disintegration rate (mCi), gamma source strength (MeV/sec), and the absorbed dose rate (m rads (C)/hr) at one meter from an unshielded point source. A breakdown of the above data as a function of gamma energy for each product isotope is available as an option. This output section also includes the decay time considered and totals of the inventory data. Simple scanning of the output will pin-point the product (s) which presents the greatest hazard and the reaction (s) which produces this product (see Appendix C).

The induced activity is calculated as a function of the duration of neutron exposure and the decay times. The effects of cyclic neutron exposure and of target atom burn-up can also be evaluated. The activity is calculated per-unit volume, per-unit mass, or for the total mass of the composite material, depending on the input specification.

ACTIVATION EQUATIONS

The build-up and decay of neutron-induced radioactivity are calculated from the equations given below which have been derived from the basic activation equations (see ref. 2). In each of the equations listed below, the term $\sigma\varphi$ represents a summation over the entire neutron energy range and is independent of time.

For an irradiation time t_1 , with zero decay time, where target atom burn-up is ignored, the induced activities are:

for the parent

$$S_1(t_1) = N\sigma\varphi \left(1 - e^{-\lambda_1 t_1} \right)$$

for the daughter

$$S_2(t_1) = \frac{N\sigma\varphi}{(\lambda_2 - \lambda_1)} \left[\lambda_2 \left(1 - e^{-\lambda_1 t_1} \right) - \lambda_1 \left(1 - e^{-\lambda_2 t_1} \right) \right] \quad (1)$$

for the granddaughter

$$S_3(t_1) = \frac{N\sigma\varphi}{(\lambda_2 - \lambda_1)} \left[(\lambda_2 - \lambda_1) \left(1 - e^{-\lambda_3 t_1} \right) - \frac{\lambda_2 \lambda_3}{(\lambda_3 - \lambda_1)} \left(e^{-\lambda_1 t_1} - e^{-\lambda_3 t_1} \right) + \frac{\lambda_1 \lambda_3}{(\lambda_3 - \lambda_2)} \left(e^{-\lambda_2 t_1} - e^{-\lambda_3 t_1} \right) \right]$$

where S_1, S_2, S_3 are the disintegration rates (dis/sec), N is the initial number of target atoms (number), σ is the activation cross section ($\text{cm}^2/\text{neutron}$), φ is the neutron flux ($\text{neutrons}/\text{cm}^2\text{-sec}$), $\lambda_1, \lambda_2, \lambda_3$ are the decay constants for the parent, daughter, and granddaughter, respectively (sec^{-1}).

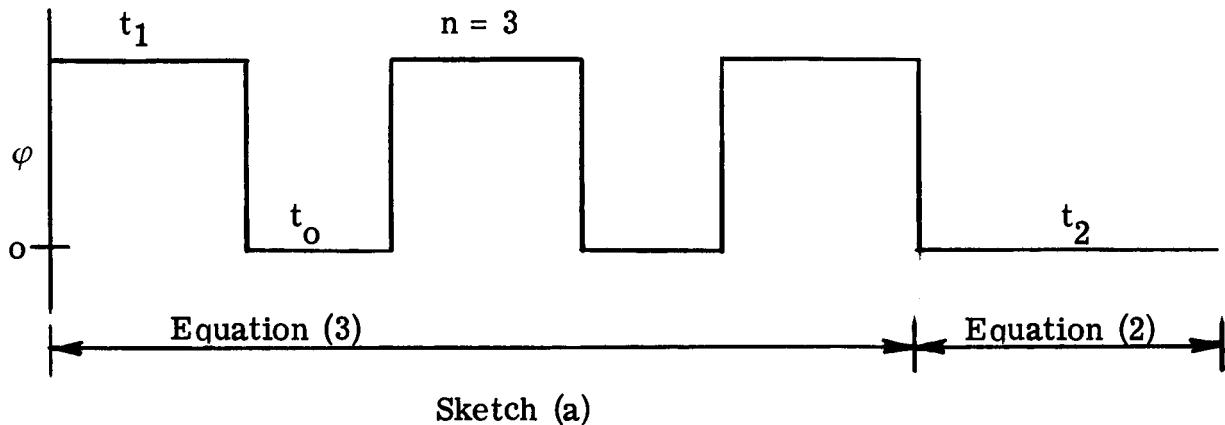
For a neutron irradiation time t_1 followed by a decay time t_2 , the induced activities are

$$\left. \begin{aligned} S_1(t_1, t_2) &= S_1(t_1)e^{-\lambda_1 t_2} \\ S_2(t_1, t_2) &= S_2(t_1)e^{-\lambda_2 t_2} + \frac{\lambda_2 S_1(t_1)}{(\lambda_2 - \lambda_1)} \left(e^{-\lambda_1 t_2} - e^{-\lambda_2 t_2} \right) \\ S_3(t_1, t_2) &= S_3(t_1)e^{-\lambda_3 t_2} + \frac{\lambda_3 S_2(t_1)}{\lambda_3 - \lambda_2} \left(e^{-\lambda_2 t_2} - e^{-\lambda_3 t_2} \right) \\ &\quad + \frac{\lambda_2 \lambda_3 S_1(t_1)}{(\lambda_2 - \lambda_1)} \left(\frac{e^{-\lambda_1 t_2} - e^{-\lambda_3 t_2}}{\lambda_3 - \lambda_1} - \frac{e^{-\lambda_2 t_2} - e^{-\lambda_3 t_2}}{\lambda_3 - \lambda_2} \right) \end{aligned} \right\} \quad (2)$$

For a cyclic neutron exposure, with zero decay time following the end of the last exposure, the induced activities, adjusted for target atom burnup, are:

$$\left. \begin{aligned} S_1 &= \frac{N\sigma\varphi\lambda_1}{\lambda_1 - \sigma\varphi} \left(e^{-\sigma\varphi t_1} - e^{-\lambda_1 t_1} \right) \left[\frac{e^{-n\sigma\varphi t_1} - e^{-n\lambda_1(t_1 + t_o)}}{e^{-\sigma\varphi t_1} - e^{-\lambda_1(t_1 + t_o)}} \right] \\ S_2 &= \frac{N\sigma\varphi\lambda_1\lambda_2}{\lambda_1 - \sigma\varphi} \left(\frac{e^{-\sigma\varphi t_1} - e^{-\lambda_2 t_1}}{\lambda_2 - \lambda_1} \right) \left[\frac{e^{-n\sigma\varphi t_1} - e^{-n\lambda_1(t_1 + t_o)}}{e^{-\sigma\varphi t_1} - e^{-\lambda_1(t_1 + t_o)}} \right] \\ S_3 &= \frac{N\sigma\varphi\lambda_1\lambda_2\lambda_3}{\lambda_1 - \sigma\varphi} \left[\left(\frac{1}{\lambda_2 - \sigma\varphi} \right) \left(\frac{e^{-\sigma\varphi t_1} - e^{-\lambda_3 t_1}}{\lambda_3 - \sigma\varphi} - \frac{e^{-\lambda_2 t_1} - e^{-\lambda_3 t_1}}{\lambda_3 - \lambda_2} \right) - \left(\frac{1}{\lambda_2 - \lambda_1} \right) \right. \\ &\quad \times \left. \left(\frac{e^{-\lambda_1 t_1} - e^{-\lambda_3 t_1}}{\lambda_3 - \lambda_1} - \frac{e^{-\lambda_2 t_1} - e^{-\lambda_3 t_1}}{\lambda_3 - \lambda_2} \right) \right] \left[\frac{e^{-n\sigma\varphi t_1} - e^{-n\lambda_1(t_1 + t_o)}}{e^{-\sigma\varphi t_1} - e^{-\lambda_1(t_1 + t_o)}} \right] \end{aligned} \right\} \quad (3)$$

where n is the number of cycles, t_1 is the irradiation time per cycle, and t_0 is the non-irradiation time per cycle. Note that equations (3) calculate the end-of-exposure activity for n cycles (n irradiation and $(n-1)$ non-irradiation periods) with burn-up. The results of these equations are then used in equations (2) to calculate the activity after decay periods following cyclic exposure. See sketch (a).



The above equations yield the disintegration rates in disintegrations per second which are then converted to the desired output quantities. The gamma ray source strength (MeV/sec) is obtained by multiplying the disintegration rate by the appropriate gamma ray energies and the fraction of gamma rays emitted at each energy per disintegration. The absorbed dose rate \dot{D} in m rads (C)/hr at one meter from an unshielded point source is calculated from

$$\dot{D} = \frac{K}{4\pi R^2} S(\text{MeV/sec}) = 1.285 \times 10^{-8} S \quad (4)$$

where K is an energy flux to dose conversion factor, R is the distance from the source (1 m), and S is the source strength. K consists of a unit conversion factor and the mass energy absorption coefficient for carbon, which was arbitrarily selected as the 1 MeV value ($0.0280 \text{ cm}^2/\text{g}$). See reference 2. Appendix A is a complete FORTRAN listing of the NAC code.

PROGRAM DESCRIPTION

The NAC data library (see appendix B) contains the activation constants for 71 naturally occurring elements with a total of 251 reactions producing 226 radioactive isotopes. For each material to be analyzed, up to 20 different elements may be specified. Provision has been made for the analysis of as many different materials, per computer run, as desired. For each analysis, up to 20 decay time intervals may be specified. The NAC data library contains the data listed below for 71 naturally occurring elements.

- (1) target element names
- (2) isotopic reaction
- (3) activation cross sections (cm^2/g)
- (4) decay constants (min^{-1})
- (5) atomic densities (atoms/g)
- (6) product isotope name
- (7) decay gamma energies (MeV)
- (8) fraction of gammas at a given energy

The elements required for a material analysis are identified, during input, by their atomic number (Z) and are listed in the data library in order of increasing Z. If an element not present in the data library is specified during input, the code will write a message identifying the element in question and then will eliminate it from the calculation. Data input for each material must also include the material density or mass, the weight fractions of the constituent elements, the irradiation and decay time, and the neutron flux in the four energy groups listed below:

- | | |
|---------|--|
| Group 1 | $0.82 \text{ MeV} < E$ |
| Group 2 | $5.5 \text{ KeV} < E < 0.82 \text{ MeV}$ |
| Group 3 | $1.1 \text{ eV} < E < 5.5 \text{ KeV}$ |
| Group 4 | $E < 1.1 \text{ eV}$ |

The cross sections, taken from references 1 and 3, have been averaged as follows: for $0 < E \leq 0.2 \text{ eV}$, a Maxwellian distribution was used; for $0.2 \text{ eV} < E \leq 0.82 \text{ MeV}$, a $1/E$ distribution was used; and for $E > 0.82 \text{ MeV}$, the U^{235} fission spectrum was used.

PROGRAM OUTPUT

The program output contains the following data in the order listed. Appendix C contains the output for 3 sample problems.

item 1: information provided by the user to identify each material;
item 2: the neutron flux in order of decreasing energy and the

irradiation time, if the cycling option is used this is the
irradiation time per cycle

item 3: messages, if any, for elements requested which are not
present in the library..

item 4: element name and weight fraction

item 5: list of reactions for the element; each followed by the disintegration rates (dis/sec) for the parent, daughter, and granddaughter at zero decay time; and the fraction of induced activity due to each neutron group in order of decreasing energy.

Items 4 and 5 are repeated for all elements in a given material. The above information appears only once for each material. The following information is repeated for each decay time.

item 6: the time after irradiation in minutes and the units in which the output is calculated: per-gram, per-cubic centimeter, or for the total mass.

item 7: the product isotope name and total disintegration rate, source strength, and absorbed dose rate.

The following three lines appear if the breakdown of the activity as a function of gamma energy is desired.

item 8: the gamma ray energies

item 9: the absorbed dose rate at each gamma energy

item 10: the source strength at each gamma energy.

The last item (11) appears regardless of the options used:

11: the total material disintegration rate, source strength, and absorbed dose rate.

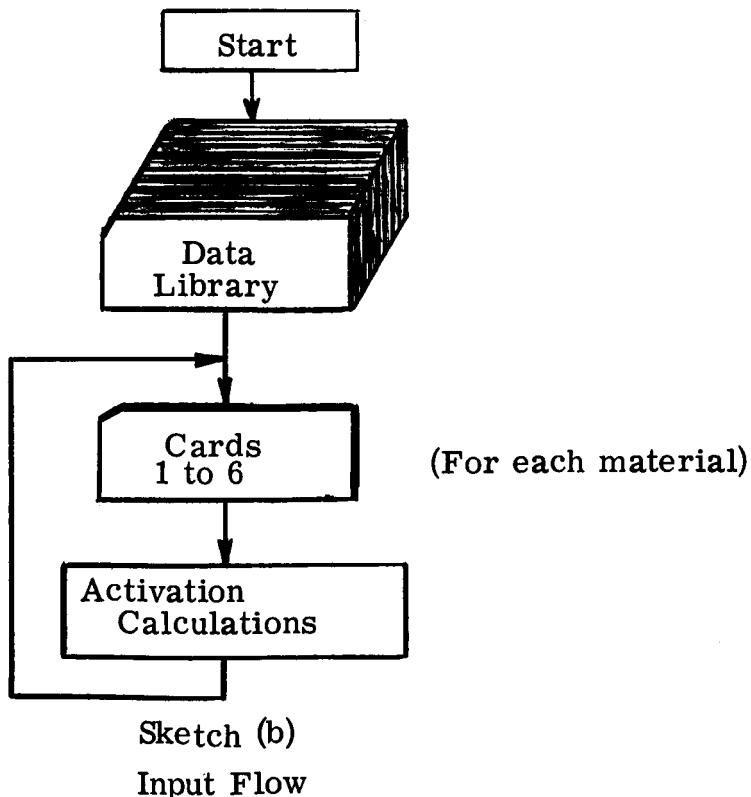
Items 6 through 11 are repeated for each time after irradiation. Those product activities which are zero (less than 10^{-38}) are not printed out.

PROGRAM LIMITATIONS

Each composite material may consist of up to 20 different elements and up to 20 different decay times may be included. The number of different materials that can be analyzed during a single computer "run" is limited only by the machine time available. All reactions for each element for which cross sections were available are included in the NAC library. These include the (n, γ) , (n, p) , (n, α) , and $(n, 2n)$ reactions; the formation of excited states and isometric states are also included. The activity for each reaction is traced through the first three generations or until a stable product is formed. However, there are some exclusions: reactions which have products having half-lives less than about one minute and products which are not gamma emitters. The dose rate contributions of alpha and beta particles are not included.

INPUT PREPARATION

Each "data link" consists of one material to be analyzed. The library data deck must precede the first data link (see sketch (b)). The number of data links that can be processed per computer run is not limited; but all the cards listed below must be present for each link.



Card no.	Columns	Data
1	FORMAT (12A6) 1-72	any information desired by user to identify the material
2	FORMAT (22I3) 3 5, 6 7-66	= 1, if the gamma energy breakdown is not desired = 2, if the gamma energy breakdown is desired the number of elements desired; the Z value for each element desired;
3	FORMAT (8F10. 4) 1-10 11-80	= 1.0, for output per gram = density (g/cm^3) for output per cm^3 = - mass, for output per total mass the weight fraction of each element in the same order as the Z values on card 2
4	FORMAT (4E10. 4) 1-40	neutron flux in order of decreasing in energy;
5	FORMAT (I3, 2E10. 4, I3) 1-3 4-13 14-23 24-26	number of reactor cycles; columns are left blank if cycling is not desired irradiation time in minutes (if cycling is desired, the irradiation time per cycle) non-irradiation time per cycle in minutes; columns are left blank if cycling is not desired the number of decay times desired
6	FORMAT (8E10. 4) 1-80	the decay times in minutes from the end of irradiation (from the end of the last exposure for cycling)

Note that card five must be used with or without cycling. Normal (non-cyclic) calculations (equations (1)) do not include target atom burn-up. Calculation of target burn-up without cycling may be obtained by setting the number of cycles to 1 and the non-irradiation time per cycle to zero on card 5.

APPENDIX A A COMPLETE FORTRAN LISTING OF THE NAC CODE

```

INTEGER OPT,Z(21),PA(251),PB(251),PC(251)
REAL LA(251),LB(251),LC(251)
DIMENSION ELEM(2,71),REAC(5,251),SIGMA(4,251),ISO(2,226),NE(226),
AEGAM(7,226),FRAC(7,226),IE(71),IDEL(71),AD(71),NAME(12),WTF(20),
BPHI(4),T(20),FN(4),PROD(50,20),IP(50),SF(4),SFX(4),S(7),R(7),DF(4)
C,DFN(4)

C
C      READ IN DATA LIBRARY
C
      READ (5,100)((ELEM(I,K),I=1,2),K=1,71)
100 FORMAT (12A6)
      READ (5,101) (IE(J),IDEL(J),J=1,71)
101 FORMAT (20I4)
      READ (5,102) (AD(J),J=1,71)
102 FORMAT (8E10.4)
      READ (5,103) ((REAC(I,J),I=1,5),(SIGMA(I,J),I=1,4),PA(J),LA(J),
APB(J),LB(J),PC(J),LC(J),J=1,251))
103 FORMAT (5A6,4E10.4/I4,E9.4,I4,E9.4,I4,E9.4)
      READ (5,104) ((ISO(I,J),I=1,2),NE(J),(EGAM(I,J),FRAC(I,J),I=1,7),
AJ=1,226)
104 FORMAT (A3,A4,I3,14F5.2)

C
C      READ IN MATERIAL DATA
C
9999 READ (5,100) (NAME(L),L=1,12)
      READ (5,105) OPT,JJ,(Z(J),J=1,JJ)
105 FORMAT (22I3)
      READ (5,106) WT,(WTF(J),J=1,JJ)
106 FORMAT (8F10.4)
      READ (5,107) (PHI(I),I=1,4),IN,T1,T2,LL,(T(L),L=1,LL)
107 FORMAT (4E10.4/I3,2E10.4,I3/(8E10.4))
TN=FLOAT(IN)
      WRITE (6,200)
200 FORMAT (1H1,2X)

C
C      WRITE INPUT DATA--MATERIAL IDENTIFICATION INFORMATION, NEUTRON
C                  FLUX, IRRADIATION TIME OR NUMBER OF CYCLES AND
C                  IRRADIATION TIME PER CYCLE
C
      WRITE (6,201) (NAME(L),L=1,12)
201 FORMAT (1H ,29X,12A6//2X)
      IF (TN.NE.0.) GO TO 1
      WRITE (6,202) (PHI(I),I=1,4),T1
202 FORMAT (13H NEUTRON FLUX,4(5X,1PE10.3),20X,16HIRRADIATION TIME,
A 1PE12.3,4H MIN//2X)
      GO TO 2
1  WRITE (6,203) (PHI(I),I=1,4),IN,T1
203 FORMAT (13H NEUTRON FLUX,4(5X,1PE10.3),10X,I4,7H CYCLES,5X,
A16HIRRADIATION TIME,1PE10.3,4H MIN//2X)

C
C      CONVERT INPUT Z TO KEY TO REACTION INDEXING PARAMETERS
C
C      TRAP ELEMENTS REQUESTED, BUT NOT IN THE LIBRARY, WRITE MESSAGE
C
      2 DO 1000 J=1,JJ

```

```

M=Z(J)
IF (M.LT.9.OR.M.EQ.10.OR.M.EQ.39.OR.M.EQ.43.OR.M.EQ.61.OR.M.EQ.68.
AND.M.EQ.76.OR.M.EQ.82.OR.M.GE.84.AND.M.LE.89.OR.M.GT.92) GO TO 11
IF (M.NE.9) GO TO 3
Z(J)=1
GO TO 1000
3 IF (M.GT.39) GO TO 4
Z(J)=Z(J)-9
GO TO 1000
4 IF (M.GT.43) GO TO 5
Z(J)=Z(J)-10
GO TO 1000
5 IF (M.GT.61) GO TO 6
Z(J)=Z(J)-11
GO TO 1000
6 IF (M.GT.68) GO TO 7
Z(J)=Z(J)-12
GO TO 1000
7 IF (M.GT.76) GO TO 8
Z(J)=Z(J)-13
GO TO 1000
8 IF (M.GT.82) GO TO 9
Z(J)=Z(J)-14
GO TO 1000
9 IF (M.NE.83) GO TO 10
Z(J)=68
GO TO 1000
10 Z(J)=Z(J)-21
GO TO 1000
11 WRITE (6,204) M
204 FORMAT (37H ELEMENT IS NOT LISTED IN LIBRARY Z=,I3//2X)
Z(J)=0
1000 CONTINUE
C
C      BEGIN CALCULATION OF END OF IRRADIATION DISINTEGRATION RATES
C
N=0
WRITE (6,205)
205 FORMAT(5X,7HELEMENT,11X,15HWEIGHT FRACTION13X,22HDPS AT ZERO DECAY
A TIME,17X,35HACTIVITY FRACTION PER NEUTRON GROUP/2X)
DO 1012 J=1,JJ
M=Z(J)
IF (M.EQ.0) GO TO 1012
KK=IE(M)
KKK=IDEL(M)+KK-1
PERC=ABS(WT*WTF(J))
C
C      WRITE ELEMENT NAME AND WEIGHT FRACTION
C
WRITE (6,206) (ELEM(I,M),I=1,2),WTF(J)
206 FORMAT (2X/5X,2A6,10X,0PF8.5//2X)
DO 1011 K=KK,KKK
TOT=0.
DO 1002 I=1,4
FN(I)=PHI(I)*SIGMA(I,K)
DFN(I)=FN(I)
1002 TOT=TOT+FN(I)
IF (TN.NE.0.) GO TO 20
C
C      ACTIVATION WITHOUT CYCLING AND BURN-UP

```

```

C
A=PERC*TOT
AL=LA(K)
ALX=EXP(-AL*T1)
IPA=PA(K)
C
C      CALCULATE PARENT POST-IRRADIATION ACTIVITY (DIS/SEC)
C
S1=A*(1.-ALX)
IF (PB(K).EQ.0) GO TO 12
BL=LB(K)
BLX=EXP(-BL*T1)
IPB=PB(K)
C
C      CALCULATE DAUGHTER POST-IRRADIATION ACTIVITY (DIS/SEC)
C
S2=A*(BL*(1.-ALX)-AL*(1.-BLX))/(BL-AL)
IF (PC(K).EQ.0) GO TO 13
CL=LC(K)
CLX=EXP(-CL*T1)
IPC=PC(K)
C
C      CALCULATE GRAND DAUGHTER POST-IRRADIATION ACTIVITY (DIS/SEC)
C
S3=A*((BL-AL)*(2.-CLX)-BL*CL*(ALX-CLX)/(CL-AL)+AL*CL*(BLX-CLX)
A/(CL-BL))/(BL-AL)
GO TO 14
12 IPB=0
S2=0.
13 IPC=0
S3=0.
C
C      CALCULATE NEUTRON GROUP ACTIVITY FRACTIONS
C
C      WRITE REACTION, POST-IRRADIATION DISINTEGRATION RATES, AND NEUTRON
C      GROUP ACTIVITY FRACTIONS
C
14 DO 1003 I=1,4
1003 DF(I)=DFN(I)/TOT
      WRITE (6,207) (REAC(I,K),I=1,5),S1,S2,S3,(DF(I),I=1,4)
207 FORMAT (10X,5A6,3(5X,1PE10.3),4(5X,0PF6.4))
C
C      CALCULATE DISINTEGRATION RATES FOR REQUIRED DECAY TIMES
C
DO 1007 L=1,LL
IF (T(L).GT.0.) GO TO 15
AT=S1
BT=S2
CT=S3
GO TO 16
15 ALT=EXP(-AL*T(L))
AT=S1*ALT
IF (IPB.EQ.0) GO TO 16
BLT=EXP(-BL*T(L))
BT=S2*BLT+BL*S1*(ALT-BLT)/(BL-AL)
IF (IPC.EQ.0) GO TO 16
CLT=EXP(-CL*T(L))
CT=S3*CLT+CL*S2*(BLT-CLT)/(CL-BL)+CL*BL*S1*((ALT-CLT)/(CL-AL)
A-(BLT-CLT)/(CL-BL))/(BL-AL)
C

```

```

C INCLUDE PARENT, DAUGHTER, GRAND DAUGHTER DISINTEGRATIONS RATES IN
C PRODUCT ISOTOPE ARRAY--(1) IF ISOTOPE IS ALREADY PRESENT, ADD TO
C TOTAL, (2) IF NEW ISOTOPE, INCLUDE IT IN ARRAY
C
16 IF (N.NE.0) GO TO 17
PROD(1,1)=AT
IP(1)=IPA
N=1
GO TO 18
17 DO 1004 NN=1,N
IF (IPA.NE.IP(NN)) GO TO 1004
PROD(NN,L)=PROD(NN,L)+AT
GO TO 18
1004 CONTINUE
N=N+1
PROD(N,L)=AT
IP(N)=IPA
18 IF (IPB.EQ.0) GO TO 1007
DO 1005 NN=1,N
IF (IPB.NE.IP(NN)) GO TO 1005
PROD(NN,L)=PROD(NN,L)+BT
GO TO 19
1005 CONTINUE
N=N+1
PROD(N,L)=BT
IP(N)=IPB
19 IF (IPC.EQ.0) GO TO 1007
DO 1006 NN=1,N
IF (IPC.NE.IP(NN)) GO TO 1006
PROD(NN,L)=PROD(NN,L)+CT
GO TO 1007
1006 CONTINUE
N=N+1
PROD(N,L)=CT
IP(N)=IPC
1007 CONTINUE
GO TO 1011
C
C ACTIVATION CALCULATION FOR CYCLING AND BURN-UP
C
20 AL=LA(K)
ALX=EXP(-AL*T1)
TOT=0.
IPA=PA(K)
S1=0.
DO 1008 I=1,4
SF(I)=60.*FN(I)/AD(M)
SFX(I)=EXP(-SF(I)*T1)
IF ((SFX(I)-ALX).NE.0.) GO TO 21
ALC=TN
DFN(I)=FN(I)*T1*ALC
GO TO 1008
C
C CALCULATE PARENT POST-IRRADIATION ACTIVITY (DIS/SEC)
C
21 ALC=(SFX(I)**TN-EXP(-TN*AL*(T1+T2)))/(SFX(I)-EXP(-AL*(T1+T2)))
DFN(I)=FN(I)*(SFX(I)-ALX)/(AL-SF(I))*ALC
1008 TOT=TOT+DFN(I)
S1=TOT*PERC*AL
IF (PB(K).EQ.0) GO TO 22

```

```

IPB=PB(K)
BL=LB(K)
BLX=EXP(-BL*T1)
S2=0.

C
C      CALCULATE DAUGHTER POST-IRRADIATION ACTIVITY (DIS/SEC)
C

DO 1009 I=1,4
1009 S2=S2+FN(I)*((SFX(I)-BLX)/(BL-SF(I))-(ALX-BLX)/(BL-AL))/(AL-SF(I))
S2=S2*PERC*AL*BL*ALC
IF (PC(K).EQ.0) GO TO 23
IPC=PC(K)
CL=LC(K)
CLX=EXP(-CL*T1)
S3=0.

C
C      CALCULATE GRAND DAUGHTER POST-IRRADIATION ACTIVITY (DIS/SEC)
C

DO 1010 I=1,4
1010 S3=S3+FN(I)*(((SFX(I)-CLX)/(CL-SF(I))-(BLX-CLX)/(CL-BL))/(BL-SF(I))
A)-((ALX-CLX)/(CL-AL)-(BLX-CLX)/(CL-BL))/(BL-AL))
S3=S3*PERC*AL*BL*CL*ALC
GO TO 14
22 IPB=0
S2=0.
23 IPC=0
S3=0.
GO TO 14

C
C      GO BACK AND CALCULATE ACTIVITY AFTER DECAY TIMES AND INCLUDE IN
C      PRODUCT ISOTOPE ARRAY
C

1011 CONTINUE
1012 CONTINUE
NEND=N
DO 1015 L=1,LL
WRITE (6,200)
CTT=0.
RTT=0.
STT=0.
IF (ABS(WT-1.).LT..00001) GO TO 24
IF (WT.LT.0.) GO TO 25

C
C      WRITE THE DECAY TIME AND UNITS FOR CALCULATION
C

WRITE (6,208) T(L)
208 FORMAT (23H TIME AFTER IRRADIATION,1PE12.4,4H MIN,20X,31HALL OUTPU
AT PER CUBIC CENTIMETER//2X)
GO TO 26
24 WRITE (6,209) T(L)
209 FORMAT (23H TIME AFTER IRRADIATION,1PE12.4,4H MIN,20X,19HALL OUTPU
AT PER GRAM//2X)
GO TO 26
25 WRITE (6,210) T(L)
210 FORMAT (23H TIME AFTER IRRADIATION,1PE12.4,4H MIN,20X,25HALL OUTPU
AT FOR TOTAL MASS//2X)

C
C      CALCULATE DISINTEGRATION RATES (MCI), SOURCE STRENGTHS (MEV/SEC),
C      DOSE RATES (MR(C)/HR), AND TOTALS
C

```

```
26 DO 1014 N=1,NEND
K=IP(N)
NN=NE(K)
IF (PROD(N,L).EQ.0.) GO TO 1014
RT=0.
ST=0.
P=PROD(N,L)
CT=P/3.7E7
DO 1013 I=1,NN
S(I)=FRAC(I,K)*EGAM(I,K)*P
R(I)=S(I)*1.285E-8
ST=ST+S(I)
1013 RT=RT+R(I)
C
C      WRITE PRODUCT ISOTOPE INVENTORY
C
        WRITE (6,211) (ISO(M,K),M=1,2),CT,RT,ST
211 FORMAT (5X,A3,A4,10X,1PE10.4,12H MILLICURIES,5X,1PE10.4,14H MR/HR
          AAT 1 M ,5X,1PE10.4,8H MEV/SEC/2X)
        IF (OPT.EQ.1) GO TO 27
        WRITE (6,212) (EGAM(I,K),I=1,NN)
212 FORMAT (12X,13HGAMMA ENERGY ,7(5X,0PF10.4))
        WRITE (6,213) (R(I),I=1,NN)
213 FORMAT (12X,13HMR/HR AT 1 M ,7(5X,1PE10.4))
        WRITE (6,214) (S(I),I=1,NN)
214 FORMAT (12X,13HMEV/SEC      ,7(5X,1PE10.4)/2X)
27 CTT=CTT+CT
RTT=RTT+RT
STT=STT+ST
1014 CONTINUE
        WRITE (6,215) CTT,RTT,STT
215 FORMAT(2X/24H TOTAL MATERIAL ACTIVITY,10X,1PE10.4,12H MILLICURIES,
          A5X,1PE10.4,14H MR/HR AT 1 M ,5X,1PE10.4,8H MEV/SEC)
1015 CONTINUE
        GO TO 9999
        END
```

APPENDIX B

DATA LIBRARY LISTING

The NAC data library is listed below in three sections. The first section contains the target element names, atomic densities, and reaction indices. The second section contains the individual reactions and reaction parameters. The third section contains the product isotopes and gamma energy yields.

Section I contains the name of each element present in the data library, in order of increasing Z, on the first 12 cards. The next 8 cards contain one pair of reaction indices for each element. The first index identifies the first reaction for an element in the reaction table listed in Section II and the second index is the number of reactions for a given element. For example, the first two pair on the first card:

- 1 → first reaction for fluorine
- 3 → three fluorine reactions
- 4 → first reaction for sodium
- 4 → four sodium reactions

The final nine cards contain the atomic density (atoms per gram) of each element in order of increasing Z.

SECTION I ELEMENT NAMES, REACTION INDICES, ATOMIC DENSITIES (ATOMS/GRAMS)

FLUORINE	SODIUM	MAGNESIUM	ALUMINUM	SILICON	PHOSPHORUS
SULFUR	CHLORINE	ARGON	POTASSIUM	CALCIUM	SCANDIUM
TITANIUM	VANADIUM	CHROMIUM	MANGANESE	IRON	COBALT
NICKEL	COPPER	ZINC	GALLIUM	GERMANIUM	ARSENIC
SELENIUM	BROMINE	KRYPTON	RUBIDIUM	STRONTIUM	ZIRCONIUM
NIOBIUM	MOLYBDENUM	RUTHENIUM	RHODIUM	PALLADIUM	SILVER
CADMIUM	INDIUM	TIN	ANTIMONY	TELLURIUM	IODINE
XENON	CESIUM	BARIUM	LANTHANUM	CERIUM	PRASEODYMIUM
NEODYMIUM	SAMARIUM	EUROPIUM	GADOLINIUM	TERBIUM	DYSPROSIUM
HOLMIUM	THULIUM	YTTERBIUM	LUTIUM	HAFNIUM	TANTALUM
TUNGSTEN	RHENIUM	IRIDIUM	PLATINUM	GOLD	MERCURY
THALLIUM	BISMUTH	THORIUM	PROTACTINIUM	URANIUM	
1 3 4 4 8 2 10 4 14 4 18 2 20 2 22 3 25 1 26 4					
30 3 33 4 37 5 42 3 45 3 48 3 51 4 55 6 61 7 68 5					
73 8 81 4 85 8 93 3 96 5 101 5 106 6 112 4 116 4 120 6					
126 2 128 7 135 2 137 1 138 3 141 5 146 7 153 3 156 5 161 6					
167 7 174 4 178 5 183 4 187 5 192 1 193 3 196 1 197 3 200 2					
202 3 205 2 207 1 208 2 210 1 211 1 212 1 213 2 215 3 218 2					
220 3 223 2 225 3 228 4 232 4 236 4 240 2 242 1 243 2 245 1					
246 6 3.164E22 2.615E22 2.477E22 2.233E22 2.145E22 1.945E22 1.879E22 1.699E22					
1.508E22 1.540E22 1.503E22 1.340E22 1.258E22 1.181E22 1.158E22 1.097E22					
1.079E22 1.022E22 1.026E22 9.471E21 9.215E21 8.644E21 8.298E21 8.042E21					
7.630E21 7.539E21 7.184E21 7.050E21 6.885E21 6.604E21 6.488E21 6.279E21					
5.926E21 5.856E21 5.641E21 5.585E21 5.359E21 5.247E21 5.079E21 4.948E21					
4.720E21 4.747E21 4.579E21 4.533E21 4.386E21 4.341E21 4.304E21 4.278E21					
4.181E21 4.000E21 3.964E21 3.841E21 3.782E21 3.703E21 3.653E21 3.555E21					
3.481E21 3.626E21 3.375E21 3.329E21 3.273E21 3.235E21 3.118E21 3.088E21					
3.058E21 3.003E21 2.945E21 2.878E21 2.591E21 2.570E21 2.529E21					

Section II consists of two cards for each of the 251 reactions. The first card contains the reaction, followed by the activation cross sections (cm^2/g) for the four neutron groups in order of decreasing energy. Blanks indicate that the particular cross section is zero or unknown. The second card contains up to three pairs of numbers, each pair corresponding to a radioactive isotope. The first number of each pair is an index which identifies the product isotope (Section III). The second number of the pair is the isotope decay constant (min^{-1}).

For example for the first three reactions:

product isotope 3 is F^{20}

product isotope 2 is O^{19}

product isotope 1 is N^{16}

SECTION II REACTION, CROSS SECTIONS (CM²/GRAM), PRODUCT ISOTOPE INDEX,
DECAY CONSTANT (MIN⁻¹)

F 19 (N,G) F 20	2.286-6	9.130-5	3.393-5	2.814-4
3 3.707+0				
F 19 (N,P) O 19	7.581-5			
2 1.435+0				
F 19 (N,A) N 16	3.786-4			
1 5.635+0				
NA 23 (N,G) NA 24	1.602-6	2.689-5	4.851-4	1.124-3
6 7.702-4				
NA 23 (N,P) NF 23	3.927-5			
4 1.019+0				
NA 23 (N,A) F 20	1.749-5			
3 3.707+0				
NA 23 (N,2N) NA 22	1.649-7			
5 5.059-7				
MG 24 (N,P) NA 24	4.279-3			
6 7.702-4				
MG 26 (N,G) MG 27	1.678-8	2.853-7	2.348-6	5.424-5
7 7.374-2				
AL 27 (N,G) AL 28	8.262-6	6.394-4	1.822-4	4.212-3
9 3.000-1				
AL 27 (N,P) MG 27	1.200-4			
7 7.374-2				
AL 27 (N,A) NA 24	2.552-5			
6 7.702-4				
AL 27 (N,2N) AL 26	5.192-4			
8 1.635-12				
SI 28 (N,P) AL 28	2.295-4			
9 3.000-1				
SI 24 (N,P) AL 29	2.703-6			
10 1.035-1				
SI 30 (N,G) SI 31	3.288-9	5.656-8	2.499-6	5.469-4
11 4.077-3				
SI 30 (N,A) MG 27	8.042-6			
7 7.374-2				
P 31 (N,P) SI 31	7.455-4			
11 4.077-3				
P 31 (N,A) AL 28	6.866-5			
9 3.000-1				
S 34 (N,A) SI 31	2.409-6			
11 4.077-3				
S 36 (N,G) S 37	2.549-11	3.527-10	1.484-8	3.598-7
12 1.375-1				
CL 35 (N,2N) CL 34M	9.585-6			
13 2.139-2				
CL 37 (N,G) CL 38	1.370-7	1.416-6	6.153-5	1.443-3
14 1.858-2				
CL 37 (N,P) S 37	2.924-8			
12 1.375-1				
A 40 (N,G) A 41	6.974-7	7.220-6	3.182-4	7.358-3
15 6.301-3				
K 39 (N,G) K 40	2.119-7	2.194-6	9.671-5	2.236-3
17 1.039-13				
K 39 (N,2N) K 38	3.830-7			

16	9.002-2			
K	41 (N,G) K 42	1.052-7	1.090-6	4.804-5
18	9.242-4	8.821-6		1.110-4
K	41 (N,A) CL 38			
14	1.858-2	5.679-5		
CA	42 (N,P) K 42			
18	9.242-4	7.832-12	8.720-11	3.845-9
CA	46 (N,G) CA 47--SC 47			1.331-7
19	1.024-4 24 1.416-4	2.331-9	2.406-8	9.752-7
CA	48 (N,G) CA 49			2.457-5
20	7.877-3	2.259-5	2.353-4	1.038-2
SC	45 (N,G) SC 46			2.399-2
23	5.729-6	4.958-6		
SC	45 (N,A) K 42			
18	9.242-4	4.336-7		
SC	45 (N,2N) SC 44M--SC 44			
21	2.003-4 22 2.962-3	5.577-7		
SC	45 (N,2N) SC 44			
22	2.962-3	1.589-5		
TI	46 (N,P) SC 46			
23	5.729-6	3.400-5		
TI	47 (N,P) SC 47			
24	1.416-4	4.312-7		
TI	48 (N,P) SC 48			
25	2.626-4	5.344-9	7.403-8	3.265-6
TI	50 (N,G) TI 51			7.551-5
26	1.197-2	1.344-10		
TI	50 (N,A) CA 47--SC 47			
19	1.024-4 24 1.416-4	1.379-5	3.966-4	1.843-3
V	51 (N,G) V 52			4.266-2
27	1.844-1	3.560-7		
V	51 (N,P) TI 51			
26	1.197-2	1.957-7		
V	51 (N,A) SC 48			
25	2.626-4	8.222-7	8.500-6	3.747-4
CR	50 (N,G) CR 51			8.670-3
24	1.733-5	3.646-9		
CR	50 (N,2N) CR 49			
28	1.650-2	2.772-5		
CR	52 (N,P) V 52			
27	1.844-1	2.505-5		
MN	55 (N,G) MN 56			9.454-3
31	4.501-3	2.740-4		1.199-1
MN	55 (N,A) V 52			
27	1.844-1	2.128-5		
MN	55 (N,2N) MN 54			
30	1.534-6	6.554-6		
FE	54 (N,P) MN 54			
30	1.534-6	8.216-5		
FE	54 (N,A) CR 51			
29	1.733-5	2.332-7		
FF	56 (N,P) MN 56			
31	4.501-3	1.698-5		
FE	58 (N,G) FF 59			
32	1.066-5	2.567-9	2.661-8	1.174-6
CO	59 (N,G) CO 60M--CO 60			5.370-4
36	6.602-2 37 2.502-7	1.244-5	2.116-4	6.346-3
CO	59 (N,G) CO 60			1.313-1
37	2.502-7	1.346-5	1.222-4	8.015-3
CO	59 (N,P) FE 59			1.641-1
		3.443-4		

32	1.066-5			
CO 59	(N,A) MN 56	1.162-6		
31	4.501-3			
CO 59	(N,2N) CO 58M--CO 58	9.577-7		
34	1.284-3 35 6.665-6			
CO 59	(N,2N) CO 58	9.577-7		
35	6.665-6			
NI 58	(N,P) CO 58M--CO 58	9.038-5		
34	1.284-3 35 6.665-6			
NI 58	(N,P) CO 58	9.119-4		
35	6.665-6			
NI 58	(N,NP) CO 57	2.973-4		
33	1.783-6			
NI 58	(N,2N) NI 57	4.358-8		
38	3.067-4			
NI 60	(N,P) CO 60	1.342-5		
37	2.502-7			
HT 62	(N,A) FE 59	5.257-8		
32	1.066-5			
NI 64	(N,G) NI 65	1.386-8	1.436-7	6.333-6
39	4.444-3			1.464-4
CU 63	(N,G) CU 64	6.810-6	1.688-4	3.418-4
41	8.887-4			4.717-3
CU 63	(N,A) CU 60	4.718-6		
37	2.502-7			
CII 63	(N,2N) CU 62	1.501-6		
40	6.974-2			
CU 65	(N,G) CU 66	1.180-5	5.629-5	5.602-4
42	1.359-1			4.355-3
CU 65	(N,2N) CU 64	1.189-6		
41	8.887-4			
ZN 64	(N,G) ZN 65	1.596-7	1.668-6	7.347-5
45	1.969-6			1.700-3
ZN 64	(N,P) CU 64	3.156-5		
41	8.887-4			
ZN 64	(N,2N) ZN 63	1.740-7		
44	1.026-2			
ZN 66	(N,P) CU 66	8.372-6		
42	1.359-1			
ZN 67	(N,P) CU 67	1.014-7		
43	1.904-4			
ZN 68	(N,G) ZN 69M	5.394-9	1.332-7	5.881-6
46	8.252-4			2.083-4
ZN 68	(N,A) NI 65	3.421-8		
39	4.444-3			
ZN 70	(N,G) ZN 71	1.569-10	3.889-9	1.714-7
47	3.151-1			3.963-6
GA 69	(N,G) GA 70	1.087-5	6.186-5	2.529-4
49	3.285-2			5.848-3
GA 69	(N,P) ZN 69M	1.166-6		
46	8.252-4			
GA 69	(N,2N) GA 68	3.107-6		
48	1.019-2			
GA 71	(N,G) GA 72	6.420-5	5.972-4	1.381-2
50	8.622-4			
GE 70	(N,P) GA 70	5.924-5		
49	3.285-2			
GE 70	(N,2N) GE 69	4.251-7		
52	2.888-5			
GE 72	(N,P) GA 72	2.271-8		

50	8.622-4				
GE 73	(m,p) GA 73	2.381-6			
51	2.407-3				
GE 74	(m,A) 79 71	1.222-5			
47	3.157-1				
GE 76	(m,G) GE 77--AS 77	8.357-10	4.091-8	1.768-6	4.088-5
55	1.050-3 58 2.962-4				
GE 76	(m,G) GE 77--AS 77	7.187-10	3.518-8	1.520-6	3.516-5
53	1.702-2 58 2.962-4				
GE 76	(m,G) GE 77--AS 77	1.170-10	4.730-9	2.480-7	4.620-6
54	1.702-2 55 1.050-3 58	2.962-4			
AS 75	(m,G) AS 76	1.809-5	1.616-4	1.199-3	2.776-2
57	4.360-4				
AS 75	(m,A) GA 72	1.733-7			
50	8.622-4				
AS 75	(m,2m) AS 74	1.816-6			
56	2.676-5				
SE 74	(m,G) SE 75	1.195-6	3.660-6	5.995-5	1.386-3
60	3.984-6				
SE 77	(m,p) AS 77	6.955-6			
58	2.985-4				
SE 80	(m,G) SE 81m		8.0186-8	3.961-6	9.153-5
61	1.220-2				
SE 82	(m,G) SE 83m--SE 83--SE 83			3.841-5	1.738-3
62	6.028-1 63 2.773-2 67	5.023-3			
SE 82	(m,G) SE 83--SE 83			1.384-4	3.043-3
63	2.773-2 67 5.023-3				
KR 74	(m,G) KR 80		2.640-6	1.124-3	2.594-2
65	3.939-2				
KR 74	(m,A) AS 76	4.882-7			
57	4.360-4				
KR 81	(m,G) KR 82	6.675-6	1.568-3	8.602-3	9.850-3
68	3.219-4				
KR 81	(m,A) AS 78	1.027-4			
69	1.617-3				
KR 81	(m,2m) KR 80--KR 80	1.526-6			
64	8.767-3 65 5.939-2				
KR 78	(m,G) KR 79	3.831-9	3.962-8	1.756-6	4.040-5
69	3.358-4				
KR 80	(m,G) KR 81	7.0154-8	2.300-7	6.778-4	1.246-2
69	6.414-12				
KR 84	(m,G) KR 85	2.231-6	3.301-4	4.448-4	6.244-5
70	2.525-3				
KR 84	(m,G) KR 85m--KR 85	4.512-6	1.407-3	2.109-3	2.662-4
70	2.526-3 71 1.238-7				
KR 84	(m,G) KR 85	7.014-6	1.048-3	1.558-3	1.472-4
71	1.238-7				
KR 86	(m,G) KR 87		5.913-8	2.603-6	6.015-5
72	8.887-3				
KR 86	(m,G) KR 86	1.529-7	4.959-6	2.148-4	3.717-3
74	2.530-5				
KR 85	(m,2m) KR 84	3.685-6			
73	1.454-5				
KR 87	(m,G) KR 88	3.659-6	2.559-5	1.285-5	1.892-4
75	3.894-2				
KR 87	(m,2m) KR 86	1.703-6			
74	2.530-5				
KR 84	(m,G) KR 85m	4.124-10	4.246-9	1.872-7	5.952-6
77	4.204-3				
KR 84	(m,G) KR 85m--KR 85	3.081-9	3.814-8	1.685-6	6.033-5

76	9.903-3	78	7.618-5				
SR 84	(N,G) SR 85			3.493-9	4.243-8	1.872-6	6.628-5
78	7.618-5						
SR 86	(N,G) SR 87M			8.522-8	8.799-7	3.885-5	8.982-4
79	4.120-3						
ZR 90	(N,2N) ZR 89			7.668-7			
84	1.453-4						
ZR 94	(N,G) ZR 95--NR95M--NR95				4.674-7	5.934-9	1.397-6
85	7.382-6	90	1.283-4	91	1.372-5		
ZR 94	(N,G) ZR 95--NR 95				2.291-5	2.909-7	6.848-5
85	7.382-6	91	1.372-5				
ZR 94	(N,A) SR 91--Y 91M--Y 91			2.321-10			
80	1.195-3	82	1.378-2	83	8.242-6		
ZR 94	(N,A) SR 91--Y 91			1.613-10			
81	1.195-3	83	8.242-6				
ZR 96	(N,G) ZR 97--NR 97			7.836-8	6.549-6	2.935-7	1.446-5
86	6.796-4	92	9.614-3				
NR 93	(N,G) NR 94M--NR 94			1.545-5	3.927-3	4.655-3	5.992-3
88	1.050-1	89	6.301-11				
NR 93	(N,2N) NR 92			3.977-8			
87	4.813-5						
M0 92	(N,G) M0 93M			5.400-8	2.298-5	1.516-6	4.000-5
93	1.650-3						
MII 92	(N,P) NR 92			1.319-6			
87	4.814-5						
MII 92	(N,A) ZR 89			1.695-8			
84	1.462-4						
MII 95	(N,P) NR 95			9.858-8			
91	1.375-5						
MII 97	(N,P) NR 97			1.744-5			
92	9.367-3						
MII 98	(N,G) M0 94			6.686-6	2.853-4	6.334-3	6.110-4
94	1.724-4						
RH100	(N,G) RH101--RH101			5.118-8	2.233-5	3.367-5	9.706-5
95	4.621-2	96	4.951-2				
RH102	(N,G) RH103			3.400-6	6.265-4	3.443-3	2.192-3
97	1.222-5						
RH104	(N,G) RH105--RH105			4.390-6	2.794-4	1.813-3	6.136-4
97	2.606-3	100	3.224-4				
RH104	(N,G) RH105M--RH105			3.306-6	4.075-4	4.224-3	8.450-2
99	1.575-1	100	3.224-4				
PD102	(N,G) PD103			1.722-8	6.760-6	1.837-5	1.742-4
101	2.876-5						
PD108	(N,G) PD109M			2.244-7	7.878-5	4.777-4	2.181-3
103	1.459-1						
PD110	(N,G) PD111--AG111M--AG111			2.438-7	1.150-4	3.036-3	1.285-4
104	3.150-2	107	5.776-1	108	6.418-5		
AG107	(N,G) AG108				1.534-5	2.342-3	1.457-2
105	2.888-1						
AG107	(N,2N) AG106M			2.421-8			
104	5.728-5						
AG109	(N,G) AG110M			3.597-7	5.848-5	3.801-5	4.746-3
106	1.904-6						
AG109	(N,P) PD109M			3.084-8			
103	1.459-1						
AG109	(N,2N) AG108			4.537-4			
105	2.888-1						
CD106	(N,G) CD107			2.040-8	9.100-6	1.933-5	5.252-5
109	1.724-3						
CD110	(N,G) CD111M			2.075-7	1.006-4	5.933-4	1.067-4

110	1.386-2				
CD114	(N,G) CD115M-CD115-IN115M	4.357-7	2.089-4	1.133-3	1.378-3
111	1.130-5 112 2.179-4 117	2.567-3			
CD114	(N,G) CD115--IN115M	5.458-8	2.662-5	1.495-4	1.752-4
112	2.179-4 117 2.567-3				
CD116	(N,G) CD117M-CD117-IN117M	1.269-7	6.186-5	1.451-4	4.895-4
113	3.983-3 114 1.386-2 119	6.080-3			
CD116	(N,2N) CD115M-CD115-IN115M	3.410-8			
111	1.130-5 112 2.179-4 117	2.567-3			
CD116	(N,2N) CD115--IN115M	3.399-8			
112	2.179-4 117 2.567-3				
IN113	(N,G) IN114M--IN114	2.610-7	4.196-5	2.478-3	9.988-3
115	9.627-6 116 5.776-1				
IN113	(N,G) IN114	9.329-9	1.496-6	8.888-5	3.569-4
116	5.776-1				
IN115	(N,G) IN116M	1.355-5	1.199-3	2.432-1	6.256-1
118	1.286-2				
IN115	(N,P) CD115--IN115M	2.014-5			
112	2.179-4 117 2.567-3				
IN115	(N,2N) IN114M--IN114	1.130-6			
115	9.627-6 116 5.776-1				
SN112	(N,G) SN113	2.885-8	1.220-5	3.500-5	5.034-5
120	4.077-6				
SN122	(N,G) SN123	9.499-8	4.304-5	8.457-5	3.064-5
121	1.754-2				
SN124	(N,G) SN125--SB125	1.205-7	5.248-5	4.757-5	4.875-5
122	7.146-2 128 4.881-7				
SB121	(N,G) SB122M	1.690-7	4.857-5	2.761-4	4.320-4
124	1.980-1				
SB121	(N,G) SB122	4.900-6	1.410-3	8.676-3	1.252-2
125	1.724-4				
SB121	(N,2N) SB120	2.041-6			
123	8.301-5				
SB123	(N,G) SB124M--SB124	2.001-8	7.850-6	6.233-5	1.017-5
126	3.300-2 127 8.023-6				
SB123	(N,G) SB124	8.334-7	3.284-4	2.110-3	4.249-3
127	8.023-6				
SB123	(N,2N) SB122	2.020-6			
125	1.724-4				
TF122	(N,G) TF123M	4.832-8	1.724-5	9.843-5	1.026-4
129	4.621-6				
TF124	(N,G) TF125M	7.835-8	3.496-5	1.405-4	1.188-3
130	8.291-6				
TF126	(N,G) TF127M--TF127	2.105-8	1.104-5	5.325-5	6.389-5
131	4.560-6 132 1.229-3				
TF126	(N,G) TF127		9.744-5	4.634-4	5.679-4
132	1.229-3				
TF128	(N,G) TF129M--TF129	1.113-8	5.406-6	8.313-6	1.809-5
133	1.429-5 134 1.034-2				
TF128	(N,G) TF129	9.982-7	4.438-5	7.198-5	1.568-4
134	1.034-2				
TF130	(N,G) TF131--I 131	4.552-7	1.065-4	1.617-4	2.886-4
135	2.795-2 140 5.924-5				
I 127	(N,G) I 128	5.530-6	1.586-3	6.754-3	2.050-2
138	2.783-2				
I 127	(N,P) I 127	7.067-9			
132	1.229-3				
I 127	(N,A) SB124	5.099-10			
127	8.023-6				
I 127	(N,2N) I 126	4.476-6			

137	3.629-5				
XE124	(N,G) XE125--I	125	6.232-7	4.313-5	2.618-4
141	6.418-4	136	8.013-6		
XE128	(N,G) XE129M		1.213-8	5.825-6	3.378-5
142	5.332-5				1.487-4
XE132	(N,G) XE133		3.333-7	1.055-4	2.507-4
143	9.145-5			1.084-5	2.081-4
XE134	(N,G) XE135			8.916-6	8.079-5
144	1.269-3				
XE136	(N,G) XE137--CS137			6.636-6	2.017-6
145	1.777-1	149	4.951-8		4.904-5
CS133	(N,G) CS134		5.815-6	1.332-3	2.113-2
147	5.975-7				9.470-2
CS133	(N,P) XE133		6.146-8		
143	9.145-5				
CS133	(N,A) I	130	7.110-9		
139	9.242-4				
CS133	(N,2N) CS132		4.755-6		
146	7.429-5				
BA132	(N,G) BA133M--BA133		1.021-8	1.910-8	5.538-6
151	1.758-7	152	2.962-4		1.702-5
BA132	(N,P) CS132		2.237-8		
146	7.764-5				
BA134	(N,G) BA135M		4.494-7	1.767-5	4.911-4
153	4.030-4				1.709-4
BA136	(N,P) CS136		5.263-10		
148	3.703-5				
BA138	(N,P) CS138		3.360-6		
150	2.153-2				
LA139	(N,G) LA140		8.950-7	2.533-4	8.192-3
154	2.876-4				3.099-2
CE138	(N,2N) CE137M--CE137		1.300-8		
155	3.398-4	156	1.327-3		
CE140	(N,G) CE141			1.112-5	3.892-5
157	1.459-5				9.476-4
CE142	(N,G) CE143			9.522-6	2.025-5
158	3.501-4				3.593-4
PR141	(N,G) PR142		8.822-7	2.448-4	2.149-3
159	5.874-4				3.884-2
ND146	(N,G) ND147--PM147		1.671-8	4.037-6	4.913-4
160	4.359-5	163	5.023-7		6.523-4
ND148	(N,G) ND149--PM149		1.328-7	2.396-5	4.913-4
161	6.080-3	164	2.179-4		6.523-4
ND150	(N,G) ND151--PM151		6.499-8	1.174-5	2.362-5
162	5.776-2	165	4.126-4		2.817-4
SM152	(N,G) SM153		6.144-7	1.826-4	1.603-2
166	2.458-4				1.200-1
SM154	(N,G) SM155		2.734-7	5.343-5	4.784-4
167	3.150-2				3.624-3
EU151	(N,G) EU152M		1.968-4	1.292-2	5.228-1
168	1.064-7				9.541+0
EU151	(N,G) EU152		4.380-5	2.874-3	1.157-1
169	1.242-3				2.121+0
EU153	(N,G) EU154			3.809-3	2.347-1
170	8.242-8				7.691-1
GD158	(N,G) GD159		8.172-7	1.402-4	2.636-3
171	6.418-4				3.062-3
GD160	(N,G) GD161		7.196-7	1.204-4	2.357-3
172	1.873-1				5.069-4
TR159	(N,G) TR160		2.208-5	4.720-3	6.125-2
					1.401-1

173	6.665-6			
DY164	(N,G) DY165M--DY165	3.320-5	1.623-3	6.807-2
174	5.545-1 175 4.916-3	1.328-5	6.497-4	2.968-2
DY165	(N,G) DY165	1.006-5	2.316-3	5.114-2
175	4.916-3	1.435-5	2.364-3	4.290-2
H0165	(N,G) H0166M	1.655-6	4.160-5	1.861-3
176	1.100-6	2.111-5	4.153-3	1.857-1
TM169	(N,G) TM170	5.698-6	4.539-4	2.290-2
177	3.726-6	1.447-7	7.097-6	3.483-4
YB168	(N,G) YB169	4.650-7	5.412-6	1.796-2
178	1.554-5	7.594-6	1.994-4	3.128-3
LU175	(N,G) LU176M	1.216-5	2.454-3	8.288-2
179	3.122-3	4.497-6	2.065-4	1.332-3
LU176	(N,G) LU177	5.583-6	1.406-4	1.691-3
180	7.183-5	6.602-10		
HF174	(N,G) HF175	5.232-6	1.854-3	4.079-2
181	6.863-6	4.204-6	9.999-4	1.770-2
HF179	(N,G) HF180M	1.968-5	1.724-3	4.565-2
182	2.100-3	6.633-4	1.448-1	3.297+1
HF180	(N,G) HF181	1.418-4	6.883-7	1.053-5
183	1.119-5	7.844-5	4.025-7	1.118-4
TA181	(N,G) TA182	3.059-7	7.279-5	6.884-4
185	4.077-6	1.646-3		
TA181	(N,2N) TA180M	5.731-6	1.210-3	1.689-2
184	1.417-3	3.293-6		
W 184	(N,G) W 185	2.614-9	6.883-7	1.586-4
187	6.245-6	7.844-5	4.025-7	6.176-4
W 186	(N,G) W187	3.059-7	7.279-5	6.884-4
188	4.813-4	1.646-3		
W 186	(N,P) TA186	5.415-4	1.210-3	1.689-2
186	6.601-2	3.293-6		
RE185	(N,G) RE186	5.731-6	1.210-3	1.689-2
189	5.291-6	2.614-9	6.883-7	1.586-4
RE187	(N,G) RE188	7.844-5	4.025-7	6.176-4
190	6.932-4	3.059-7	7.279-5	6.884-4
IR191	(N,G) IR192M--IR192	7.312-6	6.398-4	1.694-2
191	4.881-1 192 6.478-6	1.968-5	1.724-3	4.483-1
IR191	(N,G) IR192	6.633-4	1.448-1	3.297+1
192	6.478-6	1.418-4	6.883-7	1.053-5
IR193	(N,G) IR194	2.614-9	4.025-7	1.118-4
193	6.080-4	7.844-5	6.884-4	7.140-4
PT192	(N,G) PT193M	3.059-7	7.279-5	6.884-4
194	1.118-4	1.646-3		
PT196	(N,G) PT197	5.731-6	1.210-3	1.689-2
195	5.415-4	2.614-9	6.883-7	1.586-4
PT198	(N,G) PT199--AU199	7.844-5	4.025-7	6.176-4
196	2.311-2 199 1.537-4	3.059-7	7.279-5	6.884-4
PT198	(N,2N) PT197	1.646-3		
195	5.415-4	5.731-6	1.210-3	1.689-2
AU197	(N,G) AU198	2.614-9	6.883-7	1.053-5
198	1.782-4	7.844-5	4.025-7	1.118-4
AU197	(N,P) PT197	3.059-7	7.279-5	6.884-4
195	5.415-4	1.646-3		
AU197	(N,A) IR194	5.731-6	1.210-3	1.689-2
193	6.080-4	2.614-9	6.883-7	1.586-4
AU197	(N,2N) AU196	7.844-5	4.025-7	6.176-4
197	7.788-5	3.059-7	7.279-5	6.884-4
HG196	(N,G) HG197M--HG197	1.646-3		
201	4.814-4 202 1.777-4	5.731-6	1.210-3	1.689-2
HG198	(N,G) HG199M	2.614-9	6.883-7	1.053-5

203	1.650-2				
HG200	(N,P) AU200	6.682-7			
200	1.444-2				
HG202	(N,G) HG203	8.949-5	2.181-6	2.008-5	3.393-3
204	1.024-5				
TL203	(N,P) HG203	1.739-9			
204	1.024-5				
TL203	(N,2N) TL202	1.112-6			
205	4.006-5				
HT209	(N,G) BI210--PA210		3.047-6	2.088-4	4.401-5
206	9.627-5 207 3.483-6				
TH232	(N,G) TH233--PA233--U233	4.535-6	8.604-4	4.838-3	1.564-2
213	3.136-2 216 1.777-5 218	1.772-8			
TH232	(N,2N) TH231--PA231	5.904-5			
211	4.501-4 214 3.916-11				
PA231	(N,G) PA232--U232--TH228	2.929-6	9.335-4	1.283-1	4.190-1
215	3.667-4 217 1.772-8 209	6.863-7			
U 234	(N,G) U235--TH231--PA231	5.726-9	5.179-8	3.755-7	8.775-6
220	1.904-15 211 4.501-4 214	3.916-11			
U 234	(N,2N) U233--TH229--RA225	4.700-11			
218	8.069-12 210 1.795-9 208	3.239-5			
U 235	(N,G) U 236--TH232	9.998-7	1.645-5	3.549-4	1.451-3
221	4.847-14 212 9.431-17				
U 235	(N,2N) U 234	2.664-7			
219	5.291-11				
U 238	(N,G) U239--NP239--PU239	1.375-4	8.644-4	6.482-3	5.449-3
223	2.949-2 225 2.038-4 226	5.415-11			
U 238	(N,2N) U237--NP237--PA233	5.404-5			
222	7.131-5 224 5.975-13.216	1.772-8			

Section III consists of one card for each of the 226 radioactive product isotopes. Each card contains the isotope name followed by the number of gamma rays emitted. The remainder of the card contains up to seven pairs of numbers. Each pair consists of a gamma ray energy (MeV) followed by the fraction of gamma rays emitted at that energy per disintegration. A few isotopes emit gammas at more than seven energies. In these cases, the lowest energy groups are averaged into a single gamma energy.

SECTION III PRODUCT ISOTOPE NAME, NUMBER OF GAMMAS, GAMMA ENERGY (MEV),
FRACTION OF GAMMAS AT A GIVEN ENERGY

N 16	3	7.1	.08	6.13	.99	2.15	.01
O 19	4	1.44	.03	1.37	.56	.2	.97 .112 .03
F 20	1	1.63	1.				
NE 23	2	1.65	.03	.44	.97		
NA 22	1	1.28	1.0				
NA 24	2	2.75	1.	1.37	1.0		
MG 27	3	1.02	.43	.834	1.	1.75	.01
AL 26	3	2.96	.003	1.83	.997	1.12	.04
AL 28	1	1.78	1.				
AL 29	2	2.43	.062	1.28	.938		
SI 31	1	1.27	.001				
S 37	1	3.09	.9				
CL 34M	5	1.45	1.	4.1	.009	3.3	.24 2.13 .751 1.16 .24
CL 38	2	2.16	.47	1.6	.31		
A 41	1	.29	.01				
K 38	1	2.16	1.				
K 40	1	1.46	.1				
K 42	2	1.53	.18	.32	.01		
CA 47	3	1.3	.93	.81	.07	.5	.07
CA 49	3	4.68	.01	4.05	.1	3.1	.89
SC 44M	1	.27	1.				
SC 44	4	2.69	.002	2.28	.002	1.5	.01 1.14 .03
SC 46	2	1.12	1.	.89	1.		
SC 47	1	.16	.7				
SC 48	3	1.31	1.	1.04	1.	.99	1.
TI 51	3	.93	.048	.61	.014	.322	.952
V 52	1	1.44	1.				
CR 49	3	.15	.14	.09	.35	.06	.15
CR 51	3	.65	.01	.33	.01	.32	.09
MN 54	1	.835	1.				
MN 56	7	3.39	.002	2.96	.004	2.66	.007 2.52 .012 2.12 .153 1.81 .296 .845 1.
FE 59	3	1.29	.43	1.1	.57	.2	.03
CO 57	2	.707	.002	.136	.998		
CO 58M	1	.025	1.				
CO 58	3	1.65	.005	.81	.016	.805	.995
CO 60M	1	.059	1.				
CO 60	2	1.33	1.	1.17	1.		
MI 57	3	1.9	.14	1.37	.86	.127	.14
MI 65	3	1.46	.29	1.1	.14	.37	.3
CII 62	3	1.17	.005	1.13	.001	.88	.003
CII 64	1	1.34	.42				
CII 66	2	1.04	.09	.83	.002		
CII 67	3	.388	.01	.184	.45	.093	.35
ZN 63	2	.97	.086	.67	.113		
ZN 65	1	1.11	.44				
ZN 69M	1	.438	1.				
ZN 71	1	.51	1.				
GA 68	4	1.88	.04	1.24	.03	1.07	.98 .81 .06
GA 70	3	1.21	.001	1.04	.004	.174	.001
GA 72	7	3.05	.01	2.4	.72	1.88	.25 1.04 .22 .835 1. .63 .34 .39 .04
GA 73	4	1.04	.01	.74	.06	.31	1. .054 .14
GF 69	7	2.04	.01	1.65	.01	1.33	.04 1.1 .39 .86 .18 .58 .15 .19 .1
GF 77M	1	.215	1.				

GE 77M	1	.159	1.
GE 77	7	2.32	.01
AS 74	7	2.2	.003
AS 76	5	2.06	.02
AS 77	4	.525	.008
AS 78	7	2.65	.01
SE 75	7	.77	.02
SE 81M	1	.103	1.
SE 83M	4	2.02	.35
SE 83	7	2.29	.1
RR 80M	2	.049	1.
RR 80	1	.62	.13
RR 82	7	1.32	.09
RR 83	2	.087	.2
KR 79	7	.3	.05
KR 81	1	.012	1.
KR 85M	1	.15	1.
KR 85	1	.514	.007
KR 87	4	2.57	.22
RR 84	3	1.9	.008
RR 86	1	1.08	.09
RR 88	7	4.87	.003
SR 85M	2	.232	.012
SR 85M	1	.15	1.
SR 85	1	.513	1.
SR 87M	1	.388	1.
SR 91	2	1.03	.508
SR 91	2	1.41	.171
Y 91M	1	.551	1.
Y 91	1	1.19	.002
ZR 89	1	.913	1.
ZR 95	2	.76	.439
ZR 97	4	1.72	.1
NB 92	3	1.83	.02
NB 94M	1	.042	1.
NB 94	2	.874	1.
NB 95M	1	.231	1.
NB 95	1	.765	1.
NB 97	2	1.02	.01
M0 93M	3	1.48	1.
M0 99	4	.78	.04
M0101	7	2.08	.16
TC101	5	.72	.01
RH103	7	.61	.065
RH105	7	1.35	.001
RH105M	1	.13	1.
RH105	1	.319	1.
PD103	4	.538	.001
PD109M	1	.19	1.
PD111	4	1.4	.08
AG106M	7	1.55	.296
AG108	3	.633	.019
AG110M	7	1.5	.4
AG111M	1	.065	1.
AG111	3	.342	.061
CD107	2	.846	.004
CD111M	2	.247	.94
CD115M	3	1.3	.01
CD115	6	.523	.24
CD117M	2	1.27	1.
		.28	1.

DY165M	1	.108	1.								
DY165	5	.715	.007	.634	.007	.362	.014	.28	.007	.095	.156
HO166M	7	.83	.106	.81	.6	.751	.144	.711	.58	.28	.31
TM170	1	.084	.24								
YB169	7	.308	.11	.198	.49	.177	.34	.131	.25	.11	.59
LU176M	1	.089	1.								
LU177	5	.321	.002	.25	.002	.208	.11	.113	.058	.072	.001
HF175	6	.432	.015	.343	.985	.319	.002	.229	.01	.114	.01
HF180M	6	.501	.16	.444	.8	.332	.93	.215	.82	.093	.16
HF181	7	.615	.003	.482	.83	.476	.02	.346	.14	.217	.005
TA180M	2	.102	.004	.093	.23						
TA182	7	1.23	.11	1.22	.28	1.19	.15	.222	.13	.122	.33
TA186	7	1.1	.1	.94	.15	.73	.75	.51	1.	.3	.25
W 185	1	0.56	.024								
W 187	6	.721	.01	.686	.3	.479	.3	.134	.31	.114	.01
RE186	3	.768	.001	.137	.202	.123	.002				
RE188	6	1.96	.01	1.78	.001	1.67	.001	1.13	.01	.633	.01
IR192M	1	.058	1.								
IR192	7	.79	.01	.6	.532	.485	.001	.417	.048	.375	.038
IR194	7	.994	.002	.939	.014	.645	.027	.622	.01	.328	.252
PT193M	2	.135	1.	.013	1.						
PT197	3	.279	.01	.191	.09	.077	.99				
PT199	7	.96	.1	.79	.1	.475	.1	.318	.1	.246	.1
AU196	3	.426	.06	.356	.94	.333	.263				
AU198	3	1.09	.002	.675	.011	.412	1.				
AU199	3	.208	.16	.158	.77	.05	.08				
AU200	3	1.6	.01	1.23	.24	.368	.29				
HG197M	2	.164	.97	.133	.97						
HG197	2	.191	.02	.077	1.						
HG199M	2	.368	1.	.159	1.						
HG203	1	.279	1.								
TL202	3	.965	.002	.523	.002	.44	.996				
BI210	1	0.	0.								
PO210	1	.804	.001								
RA225	1	.04	.63								
TH228	4	.214	.5	.167	.01	.132	.029	.085	.29		
TH229	2	.2	.75	.148	.25						
TH231	5	.163	.02	.069	.2	.025	.13	.018	.2		
TH232	2	.79	.2	.059	1.						
TH233	5	.67	.003	.453	.01	.195	.01	.057	.01	.029	.02
PA231	6	.3	.2	.074	.2	.053	.2	.044	.2	.028	.2
PA232	5	.584	.2	.455	.2	.389	.2	.109	.2	.047	.2
PA233	5	.476	.2	.341	.2	.313	.85	.272	.2	.016	.2
U 232	5	.33	.06	.268	.001	.131	.001	.13	.001	.058	.002
U 233	2	.056	.001	.043	.01						
U 234	2	.117	.003	.05	.28						
U 235	7	.367	.04	.289	.07	.177	.55	.165	.04	.146	.12
U 236	1	.05	.27								
U 237	7	.644	.2	.371	.2	.367	.2	.267	.2	.06	.2
U 239	1	.074	1.								
NP237	6	.2	.003	.175	.001	.15	.008	.087	.14	.057	.2
NP239	5	.94	.1	.925	.1	.871	.1	.102	.1	.044	.1
PW239	3	.124	.15	.051	.11	.013	.17				

APPENDIX C

SAMPLE PROBLEMS

The input data and the code output are presented below for three sample problems. These problems will include all of the features available in NAC. The three materials were analyzed in a single computer run and execution time was 0.14 minutes.

Each of the problems will use the same neutron flux:

$$\text{Group 1 } 3.0 \times 10^{12}$$

$$\text{Group 2 } 1.5 \times 10^{13}$$

$$\text{Group 3 } 2.7 \times 10^{13}$$

$$\text{Group 4 } 4.0 \times 10^{13}$$

Sample problem I: Aluminum 6063

Calculate the induced activity per gram for an irradiation period of 10 days with decay times of 0, 1 hour, 1 day, and 10 days

Composition (weight fraction):

Aluminum	.9765
Magnesium	.009
Silicon	.006
Iron	.0035
Copper	.001
Manganese	.001
Chromium	.001
Zinc	.001
Titanium	.001

Sample problem II: Stainless Steel 304L

Calculate the induced activity per cm^3 for an irradiation of 10 days with zero decay time. Perform gamma energy breakdown.

Density: 7.75 gram per-cubic centimeter

Composition (weight fraction):

Iron	.6412
Chromium	.200
Nickel	.12
Manganese	.02
Silicon	.01
Carbon	.008

Sample problem III: Experimental capsule

Calculate the induced activity for a total mass of 653.0 grams for an exposure of 5 cycles consisting of 10 days irradiation and 2 days non-irradiation with zero decay time.

Composition (weight fraction):

Tungsten	.151
Tantalum	.0583
Nickel	.495
Iron	.0743
Chromium	.0942
Aluminum	.127

INPUT DATA FOR THE THREE SAMPLE PROBLEMS, ILLUSTRATING THE CARD FORMAT

SAMPLE PROBLEM I ALUMINUM 6063					
1	9	13	12	14	26
				29	25
				24	30
				22	
1.0			.9765		.009
.001			.001		
3.0E+12			1.5E+13		2.7E+13
					4.0E+13
1.44E+4					4
0.0E+0			6.0E+1		1.44E+3
					1.44E+4

SAMPLE PROBLEM II STAINLESS STEEL 304 L					
2	6	26	24	28	25
				14	6
7.75				.6412	.20
3.0E+12				1.5E+13	2.7E+13
					4.0E+13
1.44E+4					1
0.0E+0					

SAMPLE PROBLEM III EXPERIMENTAL CAPSULE					
1	6	74	73	28	26
				24	13
-653.				.151	.0583
3.0E+12				1.5E+13	2.7E+13
					4.0E+13
5	1.44E+4			2.88E+3	1
0.0E+0					

SAMPLE NUMBER 1		ALUMINUM 6063		IRRADIATION TIME 1.440E 04 MIN	
NEUTRON FLUX		1.000E 12		1.000E 13	
FLUX FRACTION		1.000E 12		1.000E 13	
ALUMINUM		1.000E 12		1.000E 13	
AL 27 (N.G) AL 26		1.78E+11	0.	0.	0.0269
AL 27 (N.P) PG 27		3.51E+10	0.	0.	0.9206
AL 27 (N.A) MA 24		7.47E+09	0.	0.	0.
AL 27 (N.ZN) AL 26		3.40E+09	0.	0.	0.
MANGANESE	C.0005CC				
MG 24 (N.P) MA 26		1.15E+08	0.	0.	0.
PG 26 (N.G) PG 27		2.01E+07	0.	0.	0.9697
SILICON	C.0006CC				
SI 28 (N.P) AL 26		4.13E+06	0.	0.	0.
SI 25 (N.P) AL 25		4.86E+04	0.	0.	0.
SI 30 (N.G) SI 31		1.31E+04	0.	0.	0.9969
SI 26 (N.A) MG 27		1.44E+03	0.	0.	0.
IRON	C.0035CC				
FE 9.4 (N.P) PN 54		1.88E+04	0.	0.	0.
FE 5.4 (N.A) CR 9.1		5.40E+02	0.	0.	0.
FE 5.6 (N.P) PN 56		1.78E+05	0.	0.	0.
FE 5.6 (N.G) FF 55		1.07E+07	0.	0.	0.9985
COOPER	C.001CC				
CL 62 (N.G) CL 64		2.00E+06	0.	0.	0.0460
CL 62 (N.A) CO 66		5.09E+01	0.	0.	0.
CL 63 (N.ZN) CL 62		4.50E+03	0.	0.	0.
CL 65 (N.G) CL 64		1.90E+08	0.	0.	0.0795
CL 65 (N.ZN) CL 64		3.56E+03	0.	0.	0.
MANGANESE	C.001CC				
MN 55 (N.G) PN 54		5.05E+04	0.	0.	0.0505
MN 54 (N.A) V 52		6.38E+04	0.	0.	0.
MN 55 (N.ZN) MN 54		4.29E+02	0.	0.	0.
CHROMIUM	C.001CC				

ZINC		ZINC		ZINC		ZINC		ZINC		ZINC	
CR 5C (N.G) CR 51	7.883+ 07	0.	0.	0.0000	0.0004	0.0283	0.9713	2	0.	0.	0.
CR 5C (N.2N) CR 45	1.C9e+ 01	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
CR 52 (N.P1) V 52	8.31n+ 04	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
C.CCCCCR		C.CCCCCR		C.CCCCCR		C.CCCCCR		C.CCCCCR		C.CCCCCR	
ZN 64 (N.G) ZN 65	1.95e+ 06	0.	0.	0.0000	0.0004	0.0283	0.9713		0.	0.	0.
ZN 64 (N.P) CL 64	9.46e+ 04	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
ZN 64 (N.2N) ZN 63	5.22e+ 02	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
ZN 66 (N.P) CU 66	2.51e+ 04	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
ZN 67 (N.P) CL 67	2.84e+ 02	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
ZN 66 (N.G) ZN 65P	8.49e+ 06	0.	0.	0.0002	0.0002	0.0187	0.9611		0.	0.	0.
ZN 66 (N.A) N1 65	1.02e+ 02	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
ZN 7C (N.G) ZN 71	1.63e+ 05	0.	0.	0.0000	0.0004	0.0284	0.9713		0.	0.	0.
C.CC11CC		C.CC11CC		C.CC11CC		C.CC11CC		C.CC11CC		C.CC11CC	
TI 46 (N.P) SC 46	3.77e+ 03	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
TI 47 (N.P) SC 47	8.87e+ 04	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
TI 46 (N.P) SC 48	1.26e+ 03	0.	0.	1.0000	0.	0.	0.		0.	0.	0.
TI 50 (N.G) TI 51	3.11e+ 06	0.	0.	0.0000	0.0004	0.0283	0.9713		0.	0.	0.
TI 5C (N.A) CA 47--SC 47	3.10e+ 01	0.	0.	2.069e-01	0.	0.	0.		0.	0.	0.

TIME AFTER IRRADIATION C. MIN

		ALL CUTPUT PER 10KAM
AT .28	4. E202E C3 PILLICLIES	4. 1n78F-34 MR/FR AT 1 M
PG .27	1.0144E C1 PILLICLIES	6. 1n40F-30 MR/FR AT 1 M
NA .24	5.142CE CC PILLICLIES	1.1n74F-31 PR/HF AT 1 M
AI .26	9.18E4E-C7 PILLICLIES	8. 1n51F-37 PR/FR AT 1 M
AI .25	1.215CF-C3 PILLICLIES	8. 1n84F-30 PR/FR AT 1 M
SI .31	2.05EF CC PILLICLIES	2.1n87F-33 PR/HF AT 1 M
PN .4	5.21CCF-C4 PILLICLIES	2.1n64F-34 MR/FR AT 1 M
CR .1	2.1312E CC PILLICLIES	3.1n13F-37 PR/FR AT 1 M
MN .6	1.366FF C2 PILLICLIES	1.1n19F-32 MR/FR AT 1 M
FE .5	2.0548E-C1 PILLICLIES	1.6n22F-31 PR/HF AT 1 M
CU .4	8.42CE CC PILLICLIES	1.6n04F-33 PR/FR AT 1 M
CG .11	1.3756E-C6 PILLICLIES	1.6n153F-30 MR/FR AT 1 M
CU .2	1.217CE-C4 PILLICLIES	5.1n65F-37 PR/HF AT 1 M
CU .6	5.1414E CC PILLICLIES	2.1n86F-31 PR/FR AT 1 M
V .52	3.5730E-C3 PILLICLIES	2.1n01F-34 PR/FR AT 1 M
CR .45	2.9562F-C7 PILLICLIES	8.1n40F-33 MR/FR AT 1 M
ZN .65	5.2896E-02 PILLICLIES	1.1n283F-32 MR/HF AT 1 M
ZN .63	1.4116E-C5 PILLICLIES	1.0n74F-30 MR/FR AT 1 M
CU .67	7.6417E-C6 PILLICLIES	4.1n103F-37 PR/FR AT 1 M
ZN .69P	2.2553E-C1 PILLICLIES	4.1n00F-32 PR/HF AT 1 M
NI .65	2.7136E-C6 PILLICLIES	9.1n36F-37 PR/HF AT 1 M
ZN .71	4.411CE-C3 PILLICLIES	1.1n39F-33 MR/FR AT 1 M
SC .44	1.0202E-C4 PILLICLIES	9.1n96F-35 MR/FR AT 1 M
SC .47	2.358CE-C3 PILLICLIES	1.1n05F-34 MR/HF AT 1 M
SC .46	2.4165E-C5 PILLICLIES	5.1n55F-33 PR/HF AT 1 M
TI .51	8.4C45E-C2 PILLICLIES	1.1n74F-32 PR/FR AT 1 M
CA .47	6.4C31E-C5 PILLICLIES	5.1n66F-33 MR/FR AT 1 M
		4.0441E-J1 MEV/SEC
		TOTAL MATERIAL ACTIVITY
		4.2221E 03 MK/mR AT 1 M
		3.0582E 11 MEV/SEC

TIME AFTER IRRADIATION & CTCR TO MIN

ALL OUTPUT PER GRAM

AL 2E	7.3544E-05 MILICURIES	6.273HF-03 PR/FR AT 1 M	4.8449E J+ MEV/SEC
BC 27	3.2C4(E-01 MILICURIES	7.4053F-02 PR/FR AT 1 M	5.7473E J+ MEV/SEC
HA 24	4.5116F CC MILICURIES	9.0194F-03 PR/FR AT 1 M	7.4859E J+ MEV/SEC
EL 26	5.1844E-01 MILICURIES	8.0151F-01 PR/FR AT 1 M	6.3853E J+ MEV/SEC
EL 25	5.6421E-06 MILICURIES	1.6175F-20 PR/FR AT 1 M	1.3210E J+ MEV/SEC
SI 21	5.7863E CC MILICURIES	1.61425F-24 PR/FR AT 1 M	1.3093E J+ MEV/SEC
PN 54	5.02C55E-04 MILICURIES	2.01882F-34 PR/FR AT 1 M	1.6095E J+ 4EV/SEC
CR 61	5.125CE 0 MILICURIES	3.01172F-32 PR/HF AT 1 M	3.0406E J+ 4EV/SEC
PN 56	1.0422E C2 MILICURIES	8.1729F-31 PR/FR AT 1 M	6.8427E J+ 4EV/SEC
FF 64	2.0529E-01 MILICURIES	1.61442F-01 PR/FR AT 1 M	1.22717E J+ MEV/SEC
CU 64	5.125CE CC MILICURIES	1.4151F-03 PR/HF AT 1 M	1.0701E 0.8 MEV/SEC
CO 66	1.3151E-06 MILICURIES	1.6152F-20 PR/HF AT 1 M	1.2726E J+ 4EV/SEC
CU 62	1.6531E-06 MILICURIES	8.01885F-19 PR/FR AT 1 M	6.5580E-J1 4EV/SEC
CU 66	1.4166E-03 MILICURIES	6.01666F-25 PR/FR AT 1 M	5.22114E J+ MEV/SEC
V 62	6.2222E-01 MILICURIES	4.01214F-28 PR/HF AT 1 M	3.3162E J+ MEV/SEC
CR 65	1.0455E-07 MILICURIES	3.0119F-39 PR/FR AT 1 M	2.4995E-J1 4EV/SEC
ZN 65	5.2665E-02 MILICURIES	1.0101F-02 PR/FR AT 1 M	9.5575E J+ MEV/SEC
ZN 63	4.4422E-06 MILICURIES	3.01009F-37 PR/FR AT 1 M	2.6155E J+ MEV/SEC
CU 67	7.6642F-06 MILICURIES	4.01017F-37 PR/FR AT 1 M	3.03546E J+ MEV/SEC
ZN 69	2.1645E-01 MILICURIES	4.01091F-32 PR/HF AT 1 M	3.5401E J+ 4EV/SEC
AI 65	2.1244E-06 MILICURIES	6.0137E-37 PR/FR AT 1 M	5.4115E J+ MEV/SEC
ZN 71	5.715CE-11 MILICURIES	6.0132F-12 PR/FR AT 1 M	5.1231E-J4 MEV/SEC
SC 66	1.0111E-04 MILICURIES	9.01004F-35 PR/HF AT 1 M	7.5848E U+ 4EV/SEC
SC 67	2.3177E-03 MILICURIES	1.01561F-14 PR/FR AT 1 M	9.8531E J+ MEV/SEC
SC 68	3.2631F-05 MILICURIES	5.013J7F-03 PR/FR AT 1 M	4.1562E J+ 4EV/SEC
TI 61	4.0448E-02 MILICURIES	7.0194F-03 PR/HF AT 1 M	5.4548E J+ 4EV/SEC
CB 67	6.2117E-05 MILICURIES	5.014HF-03 PR/HF AT 1 M	4.0193E-J1 MEV/SEC
TOTAL MATERIAL ACTIVITY	1.2000E C2 MILLICURIES	9.9267E 01 MH/MK AT 1 M	7.1220E 09 MEV/SEC

TIME AFTER IRRADIATION 1.44ECE (3 MIN)

ALL CUTOUT PER 10KAM

NA 24	1.65E+00 CC MILLICIFIES	3.4231E-01 PR/FR AT 1 M	2.5861E-01 MEV/SEC
AI 26	5.18E+00 C7 MILLICIFIES	8.8112E-01 PR/FR AT 1 M	6.3853E-01 MEV/SEC
SI 21	1.0C24E+C2 MILLICIFIES	6.0502E-01 PR/FR AT 1 M	4.7161E-01 MEV/SEC
PN 54	5.15E5E+C4 MILLICIFIES	2.0538E-01 PR/FR AT 1 M	1.6061E-01 MEV/SEC
CR 51	2.0C17E CC MILLICIFIES	3.0549E-01 PR/FR AT 1 M	2.9668E-01 MEV/SEC
PN 56	2.0C534E-C1 MILLICIFIES	1.7543E-01 PR/FR AT 1 M	1.3733E-01 MEV/SEC
RF 55	2.0E16E-C1 MILLICIFIES	1.6503E-01 PR/FR AT 1 M	1.2532E-01 MEV/SEC
CU 64	1.5C15E CC MILLICIFIES	4.0539E-01 PR/FR AT 1 M	3.1392E-01 MEV/SEC
CO 60	1.37E3E-C6 MILLICIFIES	1.6547E-01 PR/FR AT 1 M	1.2721E-01 MEV/SEC
CR 45	1.41E7E-17 MILLICIFIES	4.05084E-01 PR/FR AT 1 M	3.2203E-11 MEV/SEC
IN 65	5.2744E-C2 MILLICIFIES	1.0548E-01 PR/FR AT 1 M	9.5316E-01 MEV/SEC
IN 62	1.2722E-17 MILLICIFIES	5.0556E-01 PR/FR AT 1 M	7.4908E-11 MEV/SEC
CU 67	5.8472E-C6 MILLICIFIES	3.0547E-01 PR/FR AT 1 M	2.5795E-01 MEV/SEC
IN 65M	6.5545E-C2 MILLICIFIES	1.05567E-02 PR/FR AT 1 M	1.1336E-01 MEV/SEC
AI 65	4.6116E-C5 MILLICIFIES	1.05094E-01 PR/FR AT 1 M	1.1746E-01 MEV/SEC
SC 66	1.0116E-C4 MILLICIFIES	9.0597E-02 PR/FR AT 1 M	7.5250E-02 MEV/SEC
SC 67	1.9554E-C3 MILLICIFIES	1.0514E-01 PR/FR AT 1 M	8.1042E-01 MEV/SEC
SC 68	2.3404E-C5 MILLICIFIES	3.05172E-05 PR/FR AT 1 M	2.8927E-03 MEV/SEC
TI 61	2.7454E-C5 MILLICIFIES	4.05061E-01 PR/FR AT 1 M	3.6546E-02 MEV/SEC
CA 67	1.2511E-C5 MILLICIFIES	4.05042E-01 PR/FR AT 1 M	3.4896E-01 MEV/SEC

TOTAL MATERIAL ACTIVITY

±.912E CC PILLIGUM IF'S 4.1254E 00 AM/HK AT 1 M 3.215E 08 MEV/SEC

TOTAL MATERIAL ACTIVITY 1.444E-07 C4 PR

ALL CUTOUT PEK 19AM

AA 24	7.643E-05 PILLICLIES	1.5134E-14 PR/FR AT 1 M	1.1657E J+ MEV/SEC
AI 26	5.188E-07 PILLICLIES	8.191E-14 PR/FR AT 1 M	6.3853E J+ MEV/SEC
SI 21	1.123E-05 PILLICLIES	6.6934E-14 PR/FR AT 1 M	5.3256E-21 MEV/SEC
PN 94	5.076E-04 PILLICLIES	2.4937E-14 PR/FR AT 1 M	1.5745E J+ MEV/SEC
CR 61	1.679E CC PILLICLIES	3.0175E-14 PR/HF AT 1 M	2.3716E J+ MEV/SEC
MN 66	5.708E-27 PILLICLIES	8.1924E-14 PR/FR AT 1 M	6.3676E-14 MEV/SEC
FF 95	2.4637E-C1 PILLICLIES	1.6252E-14 PR/FR AT 1 M	1.3915E J+ MEV/SEC
CU 64	1.5666E-05 PILLICLIES	4.0152E-14 PR/FR AT 1 M	3.1247E J+ MEV/SEC
CO 60	1.318E-06 PILLICLIES	1.594E-14 PR/HF AT 1 M	1.2680E J+ MEV/SEC
ZN 65	5.1617E-C2 PILLICLIES	1.439E-14 PR/FR AT 1 M	6.2294E J+ MEV/SEC
CU 67	4.567E-C7 PILLICLIES	2.4055E-14 PR/FR AT 1 M	2.1871E J+ MEV/SEC
ZN 65M	1.656E-C6 PILLICLIES	3.4116E-14 PR/FR AT 1 M	2.5695E J+ MEV/SEC
AI 65	4.4712E-04 PILLICLIES	1.4554E-14 PR/FR AT 1 M	1.1404E-20 MEV/SEC
SC 46	5.3543E-05 PILLICLIES	8.4777E-14 PR/HF AT 1 M	6.9866E J+ MEV/SEC
SC 47	3.1211E-C4 PILLICLIES	1.5205E-14 PR/HF AT 1 M	1.2934E J+ MEV/SEC
SC 48	7.782E-C7 PILLICLIES	1.3165E-14 PR/HF AT 1 M	9.6222E J+ MEV/SEC
CA 47	1.5233E-05 PILLICLIES	1.1694E-14 PR/HF AT 1 M	9.2561E-J+ MEV/SEC

TOTAL MATERIAL ACTIVITY 1.5612E CC PILLICLIES 1.8314E-C1 MEV/SEC AT 1 M 1.0422E 07 MEV/SEC

SAMPLE FFCELEP II

STAINLESS STEEL 304

NEUTRON FLUX 2.000E 12 1.000E 13 2.000E 13 4.000E 13 IRRADIATION TIME 1.440E 04 MIN

FLFMFNT IS NOT LISTED IN LIBRARY $\tau = \epsilon$

HEIGHT FRACTION

INPS AI / EERC DECAY TIME

IRCA

C.0412C

FF 54 (N,P) PN 54	2.67E+07	0.	1.0000	C.	0.	0.
FE 54 (N,A) CR 51	7.67E+05	0.	1.0000	C.	0.	0.
FF 55 (N,P) PN 55	2.53E+08	0.	1.0000	C.	0.	0.
FF 55 (N,G) FF 55	1.52E+10	0.	0.0000	C.	0.0015	0.9985

CHROMIUM

C.2CCCC

CR 54 (N,G) CR 51	1.22E+11	0.	0.0000	C.	0.0283	0.9713
CR 55 (N,ZN) CR 45	1.69E+04	0.	1.0000	C.	0.	0.
CR 52 (N,P) V 52	1.28E+07	0.	1.0000	C.	0.	0.

NICKEL

C.1200C

Ni 54 (N,P) CC 54P--CC 54	1.52E+08	2.18E+07	1.0000	C.	0.	0.
Ni 54 (N,P) CO 54	2.32E+08	0.	1.0000	C.	0.	0.
Ni 54 (N,NP) CC 54	2.10E+07	0.	1.0000	C.	0.	0.
Ni 54 (N,ZN) Ni 54	1.20E+05	0.	1.0000	C.	0.	0.
Ni 54 (N,P) CO 54	1.34E+05	0.	1.0000	C.	0.	0.
Ni 54 (N,A) FE 54	2.08E+04	0.	1.0000	C.	0.	0.
Ni 54 (N,G) Ni 54	5.60E+04	0.	0.0000	C.	0.0283	0.9713

MANGANESE

C.02CCC

Mn 55 (N,G) PN 56	7.83E+11	0.	0.0000	C.	0.0011	0.0505
Mn 55 (N,A) V 52	9.89E+06	0.	1.0000	C.	0.	0.
Mn 55 (N,ZN) Mn 54	6.65E+04	0.	1.0000	C.	0.	0.

SILVER

C.C10CC

SI 28 (N,P) Al 28	5.33E+07	0.	1.0000	C.	0.	0.
SI 25 (N,P) Al 25	6.28E+05	0.	0.0000	C.	0.	0.
SI 25 (N,G) Si 21	1.70E+09	0.	0.0000	C.	0.0031	0.9969
SI 25 (N,A) PG 27	1.87E+06	0.	0.0000	C.	0.	0.

TIME AFTER IRRADIATION (s)

ALL CUT/FIT PEAK LJDIC CENTER

PN :4	1.7E3F-C1 MILLCIFIES	2.MR d4F-011 MR/R AT 1 M	2.2400E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	2.0E4E-C1 2.2400E C1	6.0E24F J1 MR/R AT 1 M	4.7175E J & MEV/SEC
CR :1	2.3E24F C3 MILLCIFIES	6.0E24F J1 MR/R AT 1 M	4.7175E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E5CC 5.0200E C1	0.0E0J0 4.5233E 01	0.0E200 3.5201E 09
PN :6	2.1114F C4 MILLCIFIES	4.0E32E J0 MR/R AT 1 M	1.3849E 1 & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	2.035CC 6.0311E C1	2.0E40U 1.0760E 02	1.0460E 10 2.0443E 11
CR :5	5.3161E C5	9.0E28J4 1.0E49F-011 MR/R AT 1 M	1.4600E 10 2.3711E 10
FE :5	4.1114E C2 MILLCIFIES	2.0E17F 02 MR/R AT 1 M	1.0068E 10 MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E4CC 1.0E43E C2	1.0E10U 1.0229E 02	0.0E000 1.01729E 00
CR :5	4.05E21E-C4 MILLCIFIES	9.0E38F C5 1.0E49F-011 MR/R AT 1 M	9.0538E 09 9.01273E C7
V :2	4.05E21E-C4 MILLCIFIES	6.0E37F-06 1.0E49F-011 MR/R AT 1 M	1.0427E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E4CC 1.0E43E C2	0.0E0J0 6.0E674-E6	0.0E000 1.05259E 02
CO :6P	3.07E12F CC MILLCIFIES	5.0E34F-02 1.0E49F-011 MR/R AT 1 M	1.0998E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E4CC 1.0E46E C2	1.0E10U 1.0229E 02	1.09607E-C6
CO :6E	6.0E15F CC MILLCIFIES	8.0E10F 02 MR/R AT 1 M	6.3040E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E4CC 1.0E46E C2	2.0E10F 02 MR/R AT 1 M	2.0942E J & MEV/SEC
CO :6	6.0E15F CC MILLCIFIES	2.0E10F 02 MR/R AT 1 M	2.0942E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E5CC 1.0E53E-C2	4.0E24J4-J2 3.0E11F J6	0.0E050 2.0402E C6
CO :7	5.0E62E-C1 MILLCIFIES	3.0E15JF-02 MR/R AT 1 M	2.08835E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E7CC 3.0E8C2E-C4	0.0E10U 3.0E674-E2	0.0E000 2.0E216E 00
NI :7	1.0E24E-C3 MILLCIFIES	2.0E10F-02 MR/R AT 1 M	1.7561E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E7CC 4.0E158E-C4	1.0E10U 1.0E18J4-03	0.0E270 2.0E44E-C5
CO :6C	2.0E25E-C3 MILLCIFIES	1.0E15JF J5 4.0E12F-011 MR/R AT 1 M	2.01357E C3 3.0E664E J & MEV/SEC
GAMMA ENERGY MR/R AT 1 M MEV/SEC	1.0E32CC 2.0E313E-C2	1.0E10U 2.0E24J4-03	1.0E110 1.0E159J4-05

NI 65	1.51E4 F C7 MILLICRIMES	4.450E-31 PR/FR AT 1 M	3.866UE J 2 MEV/SEC
GAMMA ENERGY	1.4ECC	1.4E00	0.2700
MR/FR AT 1 M	2.0557E C1	1.109E-01	7.997E 00
MEV/SEC	2.3741E C5	8.635E-05	6.2239E 08
AL 2P	1.4421E C1 MILLICRIMES	1.1205E-01 PR/FR AT 1 M	9.4979E J 1 MEV/SEC
GAMMA ENERGY	1.7ECC		
MR/FR AT 1 M	1.2215E CC		
MEV/SEC	0.4715E C1		
AL 2C	1.6555FF-C7 MILLICRIMES	1.1212E-02 PR/FR AT 1 M	8.4922E J 2 MEV/SEC
GAMMA ENERGY	2.4ECC	1.1E00	
MR/FR AT 1 M	1.2167E-C3	9.665E-03	
MEV/SEC	0.46E2E C4	7.545E-05	
SI 21	4.5564E C1 MILLICRIMES	2.1134E-02 PR/FR AT 1 M	2.1599E J 0 MEV/SEC
GAMMA ENERGY	1.27CC		
MR/FR AT 1 M	2.7154E-C2		
MEV/SEC	2.1555E C6		
MG 27	5.0524E-02 MILLICRIMES	3.0497E-02 PR/FR AT 1 M	2.4122E J 0 MEV/SEC
GAMMA ENERGY	1.02CC	0.0440	1.7500
MR/FR AT 1 M	1.0538E-C2	2.0034E-02	4.2946E-04
MEV/SEC	0.2011E C5	1.5534E-06	3.2771E C4
TOTAL MATERIAL ACTIVITY	2.5124E C4 MILLICRIMES	1.8209E 04 MKS/SEC AT 1 M	1.4470E 12 MEV/SEC

SAMPLE EFFECTIVE III

EXPERIMENTAL CAPSULE

NEUTRON FILE	3.000E 12	1.500E 13	2.000E 14	4.000E 15	→ CYCLES	IRRADIATION TIME 1.440E 04 MIN
EFFICIENCY	HEIGHT FRACTION	HPS AT 7 ESR DECAY TIME			ACTIVITY FRACTION PER NEUTRON GROUP	
TUNING	C.151CC					
b 184 (N.G) b 185 b 186 (N.G) b 187 b 187 (N.P) b 188	3.57E+12 1.07E+14 1.95E+15	0. 0. 0.	0. 0. 0.	0.00000 0.00000 1.00000	0.0295 0.0018 0.	0.3473 0.0418 0.
TA181 (N.G) TA182 TA181 (N.2N) TA182P	4.22E+13 5.12E+16	0. 0.	0. 0.	0.00000 1.00000	0.0082 0.	0.4949 0.
NICKEL	C.455CC					
NI 55 (N.P) CO 58P--CC 58 NI 55 (N.P) CO 58 Ni 55 (N.P) CC 57 Ni 55 (N.2N) Ni 57 Ni 55 (N.P) CC 57 Ni 55 (N.A) FF 55 Ni 54 (N.G) Ni 55	8.76E+10 3.22E+11 2.43E+10 4.19E+07 2.32E+08 2.59E+07 1.94E+12	7.605E 09 0. 0. 0. 0. 0. 0. 0.	0. 0. 0. 0. 0. 0. 0.	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0000	C. C. C. C. C. C. C.	0. 0. 0. 0. 0. 0. 0.
IRON	C.0743C					
FE 54 (N.P) PN 54 FE 54 (N.A) CR 51 FF 56 (N.P) PN 56 FF 56 (N.G) FE 55	1.24E+09 2.24E+07 2.47E+04 5.31E+11	0. 0. 0. 0.	0. 0. 0. 0.	1.0000 1.0000 1.0000 0.0000	C. C. C. C.	0. 0. 0. 0.
ALUMINUM	C.127CC					
CR 55 (N.G) CR 51 CR 55 (N.2N) CR 45 CR 52 (N.P) V 52	1.45E+13 6.72E+05 5.11E+09	0. 0. 0.	0. 0. 0.	0.00000 1.00000 1.00000	C.00004 0. C.	0.0283 0. 0.
AL 27 (N.G) AL 26 AL 27 (N.P) PG 27 AL 27 (N.A) RA 24 AL 27 (N.2N) AL 26	1.51E+13 2.98E+10 6.34E+09 1.35E+04	0. 0. 0. 0.	0. 0. 0. 0.	0.00524 1.00000 1.00000 1.00000	0.0269 0. 0. 0.	0.9206 0. 0. 0.

TIME AFTER IRRADIATION t.

MIN

ALL OUTPUT FOR INITIAL MASS

W 146	5.6737E C4 MILLCIFIES	6.1315F 37 PR/FR AT 1 M	4.8105E 1U MEV/SEC
b 147	2.9111E C6 MILLCIFIES	5.6109F 05 PR/FR AT 1 M	4.5345E 1.5 MEV/SEC
TA1E6	5.2762F-C3 MILLCIFIES	4.0322F-31 PR/FR AT 1 M	3.1535E J.5 MEV/SEC
TA1E2	1.1144E C6 MILLCIFIES	4.4172F 37 PR/FR AT 1 M	3.4375E 1.5 MEV/SEC
TA1E8H	1.2881E C1 MILLCIFIES	1.4186F-31 PR/FR AT 1 M	1.1195E 0.7 MEV/SEC
(n 15H	2.2267E C3 MILLCIFIES	2.4112F 01 PR/FR AT 1 M	2.1910E J.4 MEV/SEC
(O 15E	5.0255E C3 MILLCIFIES	3.1109F 03 PR/HF AT 1 M	2.7400E 1.1 MEV/SEC
(O 15I	5.2544E C2 MILLCIFIES	6.0121F 31 PR/FR AT 1 M	4.7160E J.4 MEV/SEC
NI 15I	1.1344E CC MILLCIFIES	7.4026E-31 PR/FR AT 1 M	6.1343E J.7 MEV/SEC
(O 15C	6.2712E C0 MILLCIFIES	7.0129F 01 PR/FR AT 1 M	5.7999E J.8 MEV/SEC
FE 15S	1.4342E C4 MILLCIFIES	8.1101F 03 PR/FR AT 1 M	6.3114E 1.1 MEV/SEC
AI 15S	5.2671E C4 MILLCIFIES	1.7139F 04 PR/FR AT 1 M	1.3416E 1.2 MEV/SEC
PN 14	5.3537E C1 MILLCIFIES	1.41102F 01 PR/FR AT 1 M	1.0352E J.9 MEV/SEC
CR 11	3.9221E C5 MILLCIFIES	7.2104F 04 PR/FR AT 1 M	5.6159E 1.1 MEV/SEC
PN 14	6.6747E C1 MILLCIFIES	5.6106F 01 PR/FR AT 1 M	4.3810E J.9 MEV/SEC
CR 14	1.8164E-C2 MILLCIFIES	5.4172F-34 PR/FR AT 1 M	4.1375E J.4 MEV/SEC
V 12	1.2825F C2 MILLCIFIES	9.4155F 01 PR/FR AT 1 M	7.3662E J.9 MEV/SEC
AL 12E	4.1114E C5 MILLCIFIES	3.4115E 05 PR/FR AT 1 M	2.7015E 1.5 MEV/SEC
PC 17	8.0555E C2 MILLCIFIES	4.4043F 37 PR/FR AT 1 M	3.8516E 1.0 MEV/SEC
NA 24	1.7111E C2 MILLCIFIES	3.4113F 32 PR/FR AT 1 M	2.6158E 1.0 MEV/SEC
AL 26	3.6666E-C4 MILLCIFIES	3.1102F-34 PR/FR AT 1 M	2.5496E J.4 MEV/SEC

TOTAL MATERIAL ACTIVITY

5.0475E C6 MILLICURIES 1.4052E C6 AM/HR AT 1 M 1.04968E 1.4 MEV/SEC

REFERENCES

1. Klopp, David A.: Prediction of Neutron Induced Activation. Vol. I: NAP Code Manual. Rep. IITRI-A6088-21, vol. 1, IIT Research Inst. (NASA CR-89654), Jan. 31, 1966.
Klopp, David A.: Prediction of Neutron Induced Activation. Vol. II: NAP, Physical Models and Experimental Validation. Rep. IITRI-A6088-22, vol. 2, IIT Research Inst. (NASA CR-89958), Jan. 31, 1966.
Klopp, David A.: Prediction of Neutron Induced Activation. Vol. III: NAP Cross Section Library. Rep. IITRI-A6088-23, vol. 3, IIT Research Inst., Jan. 31, 1966.
Klopp, David A.: Prediction of Neutron Induced Activation. Vol. IV: NAP Gamma Radiation Library. Rep. IITRI-A6088-24, vol. 4, IIT Research Inst., Jan. 31, 1966.
2. Etherington, Harold, ed.: Nuclear Engineering Handbook. McGraw-Hill Book Co., Inc., 1958.
3. Heiser, P. C.; and Ricks, L. O.: Activation Source Strength Program. ACT-II. Rep: WANL-TNR-063 (Add. 1), Westinghouse Elec. Corp., 1962.